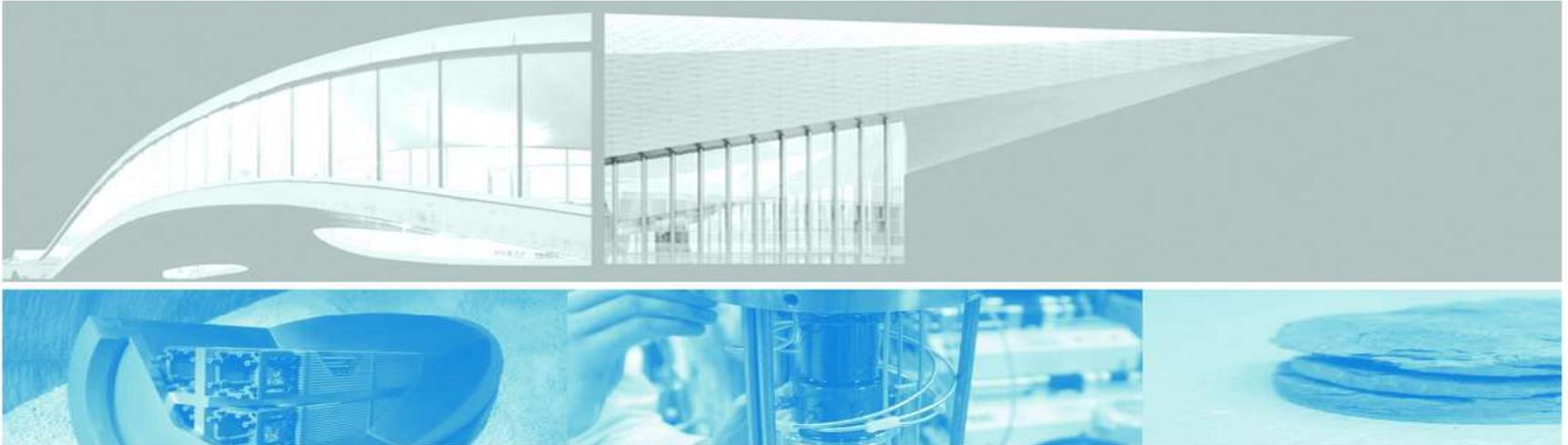


LABORATORY CHARACTERIZATION OF BENTONITE



Alessio Ferrari, Donatella Manca, Ali Seiphoori, Aldo Madaschi and Lyesse Laloui

Laboratory for Soil Mechanics
Swiss Federal Institute of Technology in Lausanne, EPFL

Mechanical Properties of Bentonite Barriers
Kaunas, 20 June 2017

Multi-barrier system (Swiss concept)

✓ High Level Waste

ENGINEERED BARRIER SYSTEM (EBS):

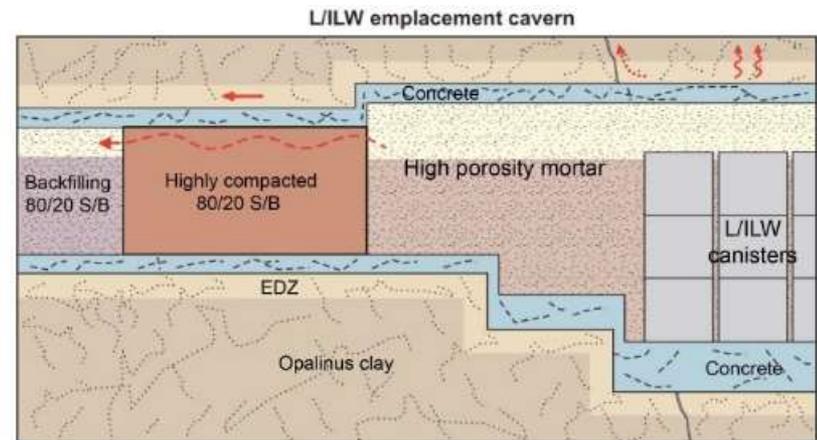
- Vitrified HLW
- Stainless steel container
- Compacted bentonite (**granular** + blocks)
- Low permeable Host rock (Opalinus Clay)



✓ Low/Intermediate Level Waste

ENGINEERED GAS TRANSPORT SYSTEM (EGTS):

- L/ILW Canister
- High porosity concrete
- Bentonite-based materials (**sand+bentonite**)
- Excavated Damage Zone in the Host rock



In the last years the Laboratory of Soil Mechanics has been involved in a series of experimental projects to focus the hydromechanical behaviour of bentonite-based materials:

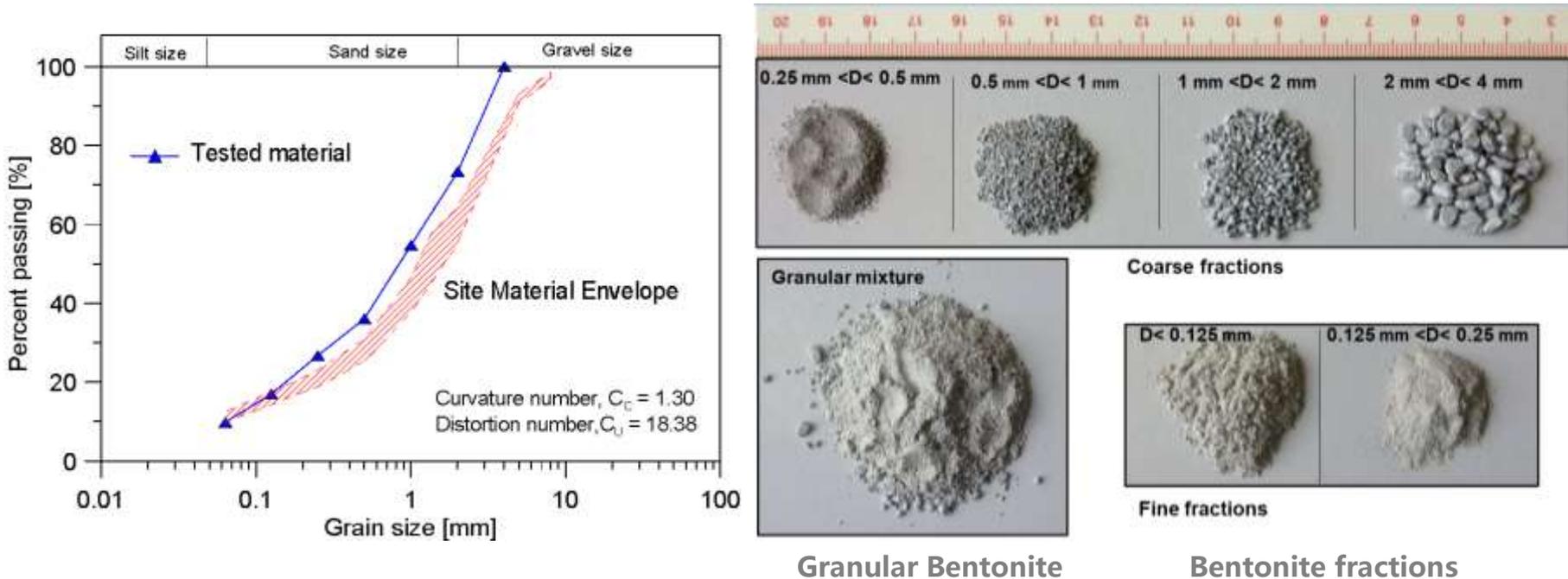
1. **MX-80 Granular Bentonite**
2. **MX-80 Granular Bentonite mixed with Quartz Sand**
3. **“Shot-clay” (Mx80 Bentonite)**

These materials have been subjected to an extensive laboratory testing program involving:

- ✓ Grain size distribution
- ✓ Microstructural and fabric characterization
- ✓ Swelling behaviour
- ✓ Water retention behaviour
- ✓ THM characterization using triaxial system

MX-80 Bentonite – Apparent Grain Size Distribution

- Mixture of different fractions of the broken and rounded bentonite units
- Grain size distribution (maximize the pourability)



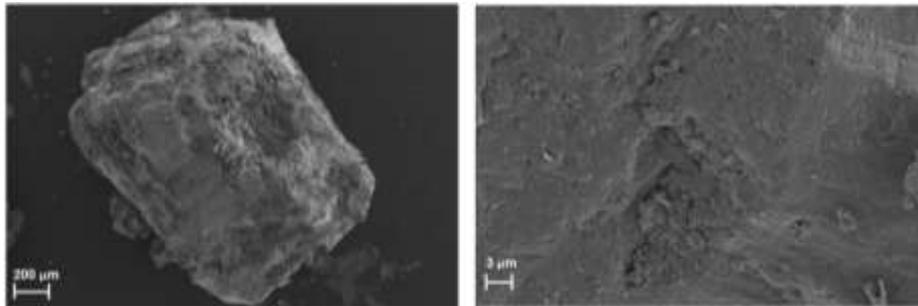
Smectite content† [%]	Specific surface area† s [m^2/g]	Specific gravity G_s	Liquid limit w_L [%]	Plastic limit w_p [%]	Hygroscopic water content (T = 22°C, RH = 34%) w_{hg} [%]
85	523	2.74	420	65	5.4

† Plötze and Weber (Nagra), 2007

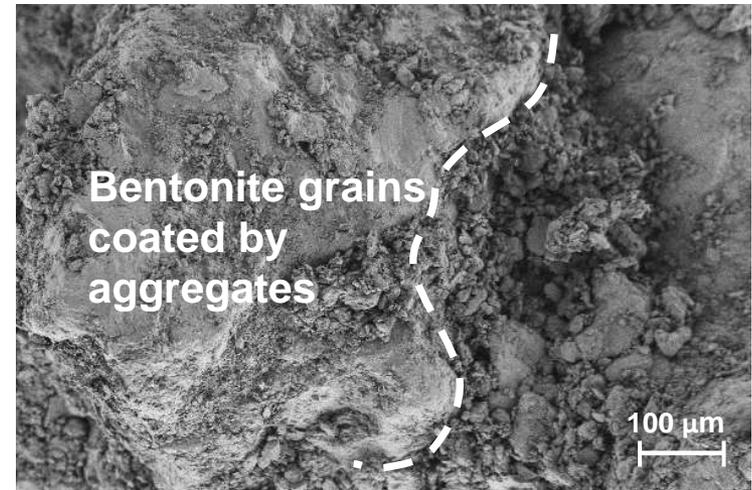
Microstructure at the as-compacted state

Seiphoori, Ferrari and Laloui (2014)

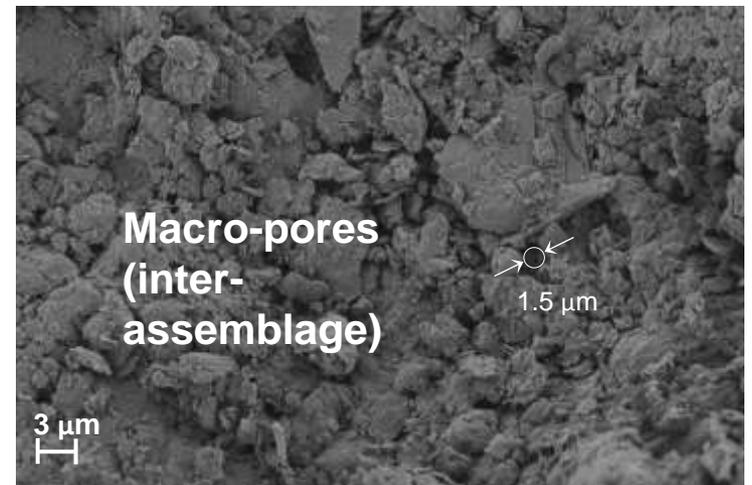
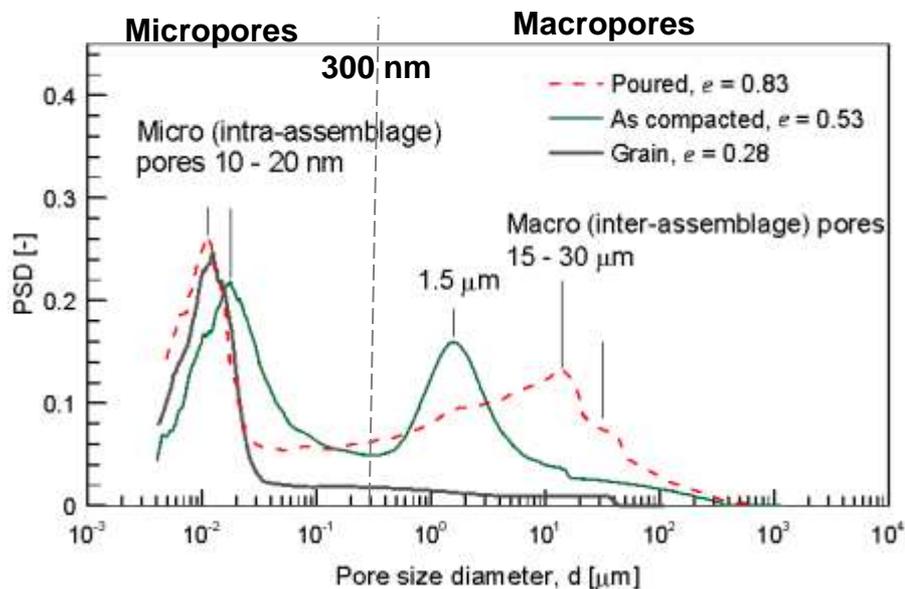
- ✓ SEM of Single Grain, $e = 0.28$, $w = 5\%$

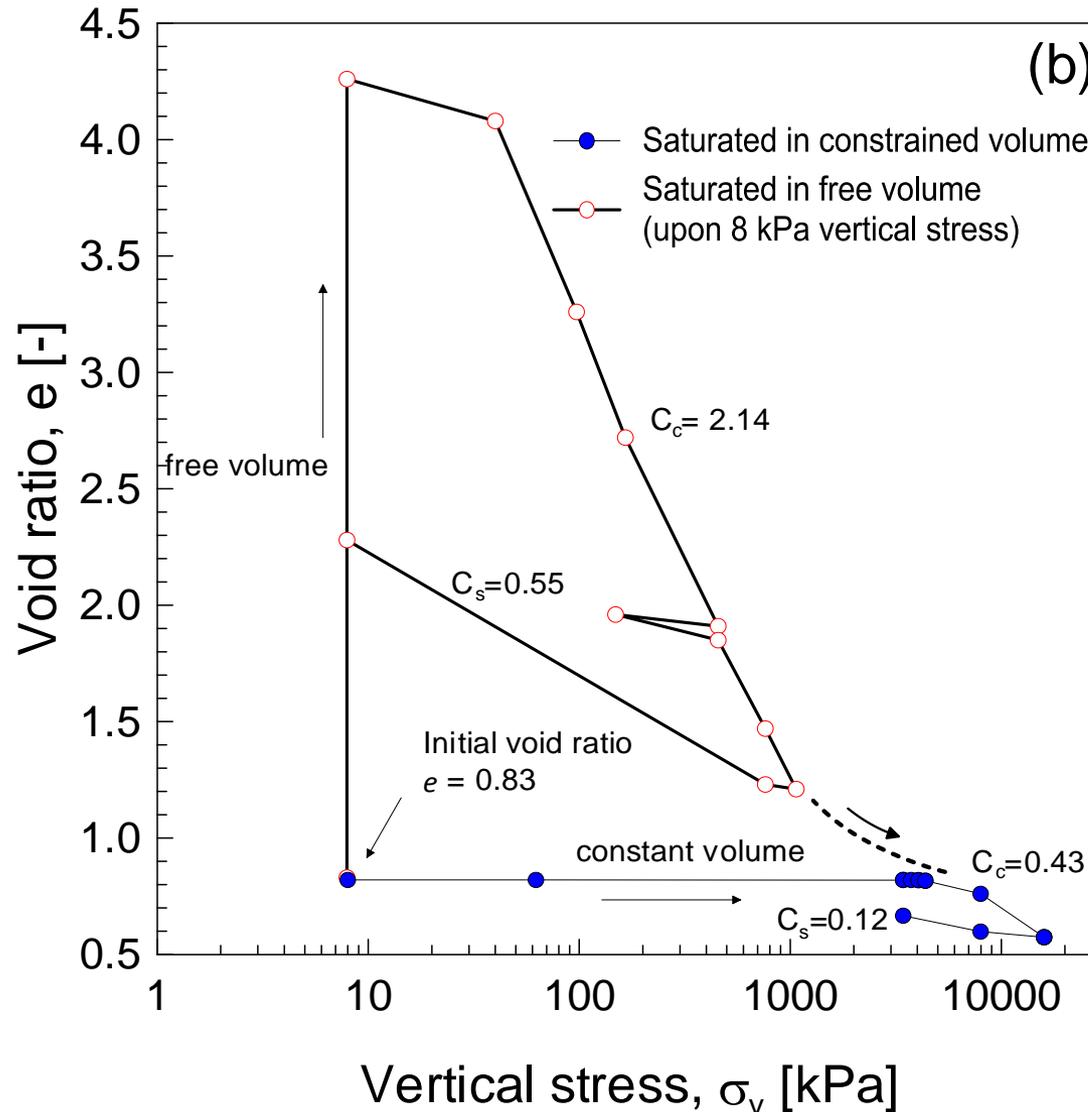


- ✓ SEM, $e = 0.53$, $rd = 1.80 \text{ Mg/m}^3$, $w = 5\%$

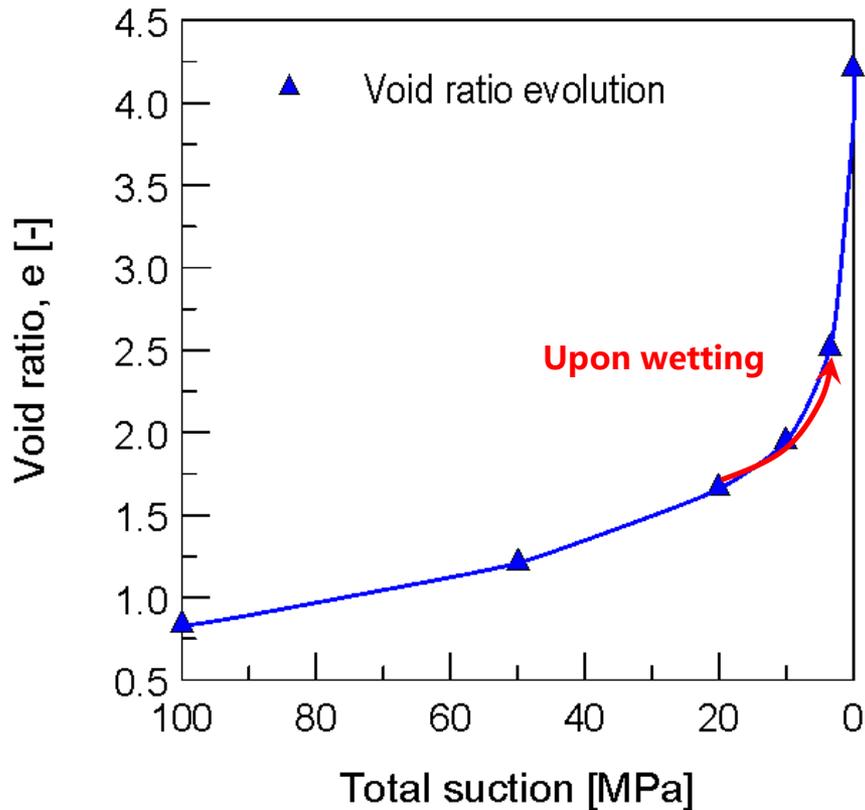


- ✓ MIP, double porosity structure

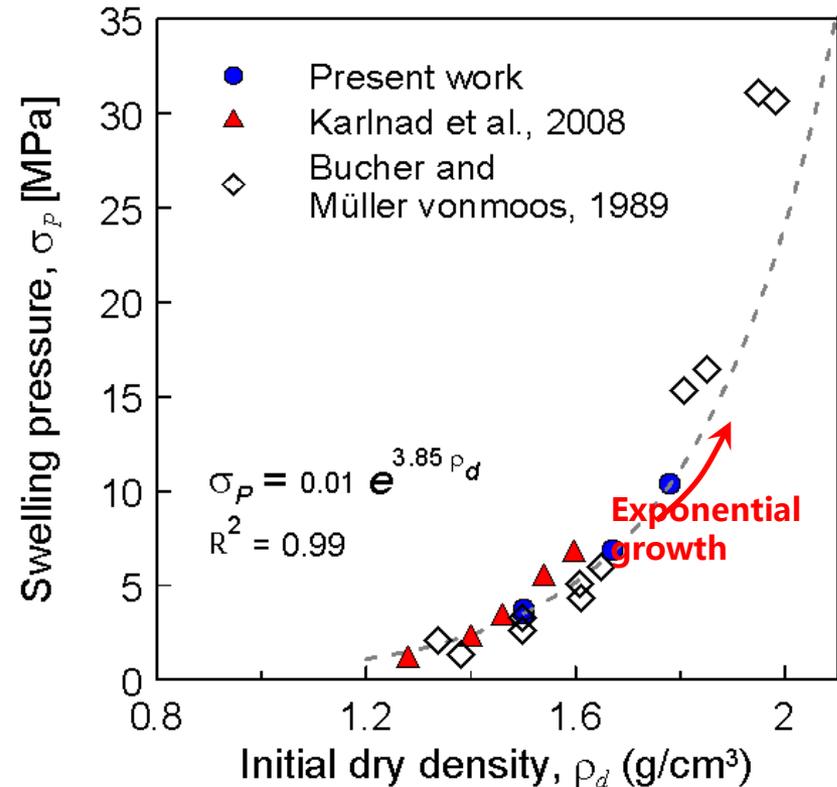




Free swelling test



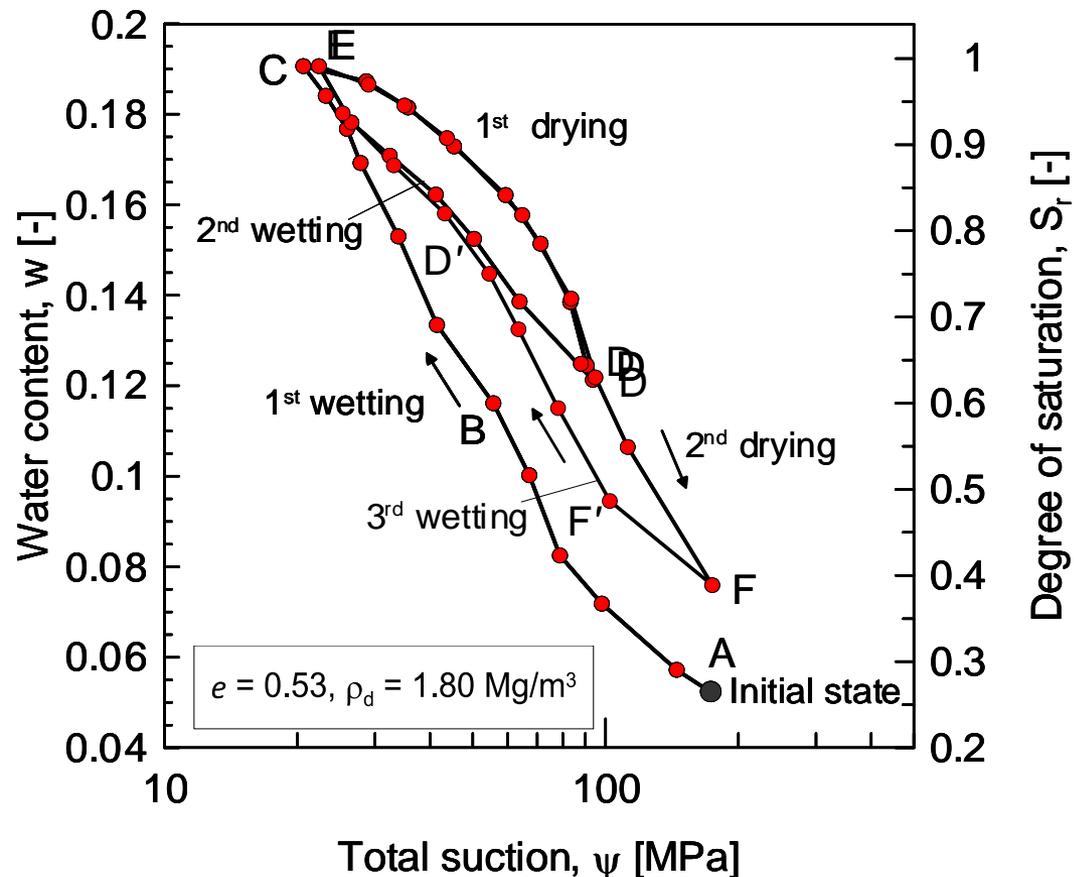
Constrained swelling test



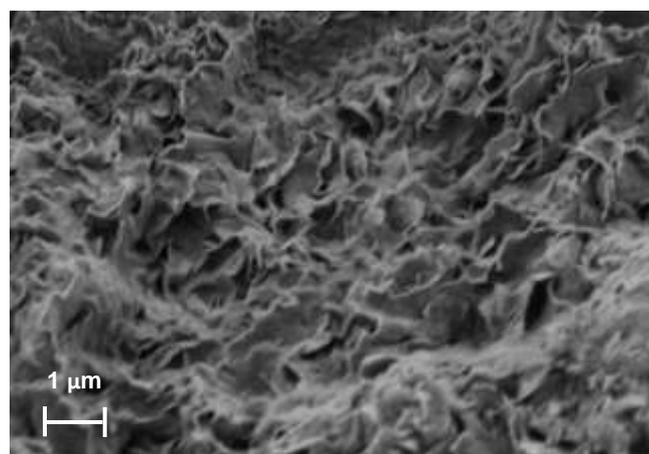
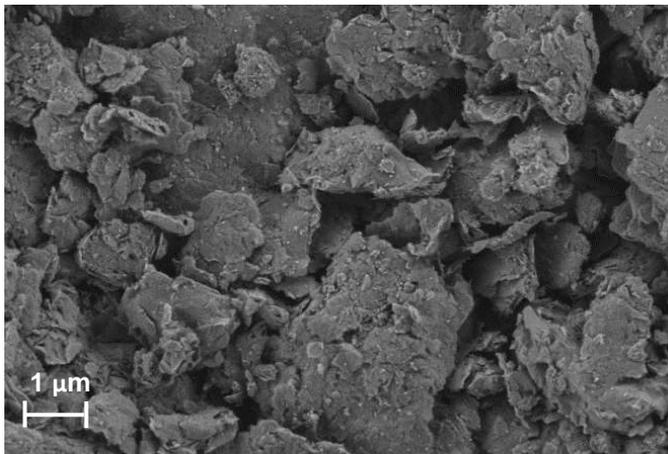
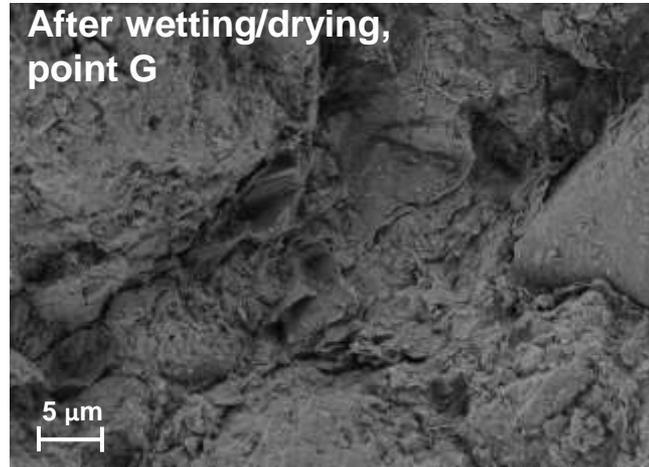
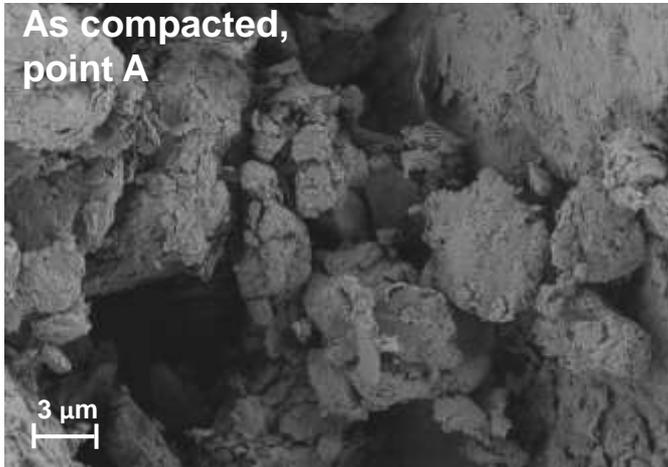
Swelling deformation up to $e = 4.2$ and swelling pressures up to **10 MPa** at $e = 0.53$ ($r_d = 1.80 \text{ Mg/m}^3$)

Wetting/drying cycles

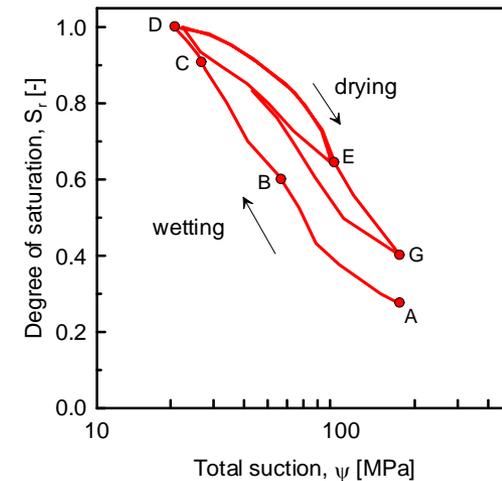
- ✓ Significant and irreversible change in water retention behaviour
- ✓ New hydraulic domain by creating a new wetting path
- ✓ Increase of the retention capacity



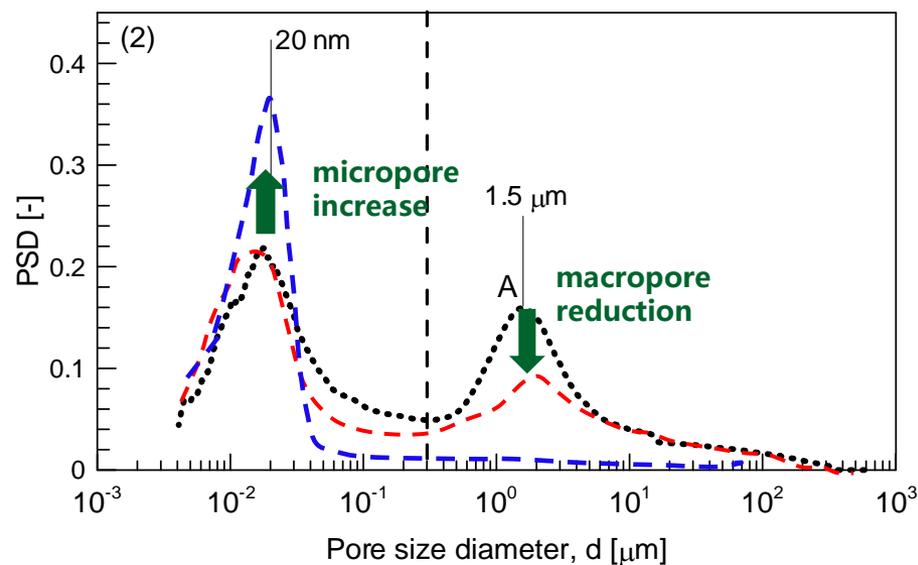
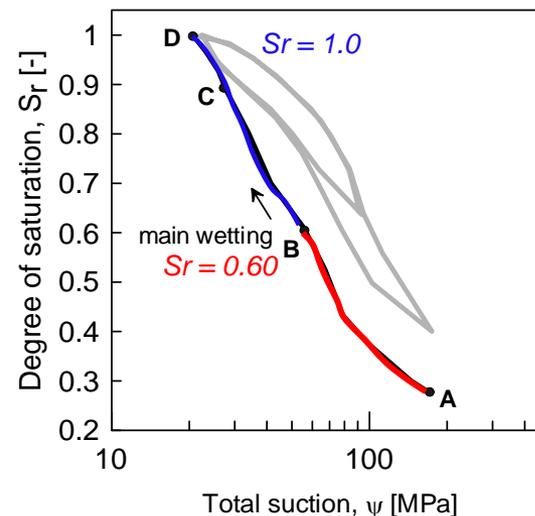
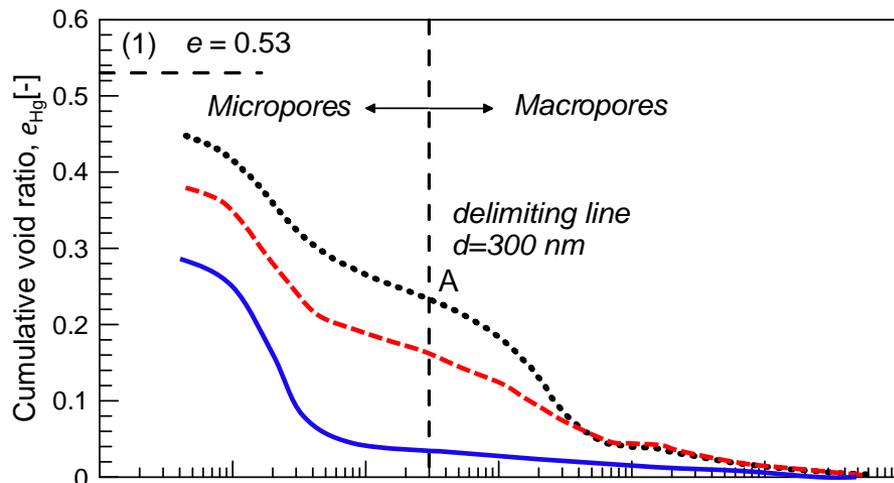
SEM analysis and the influence of wetting/drying on the fabric



Significant change of the fabric after wetting/drying cycle



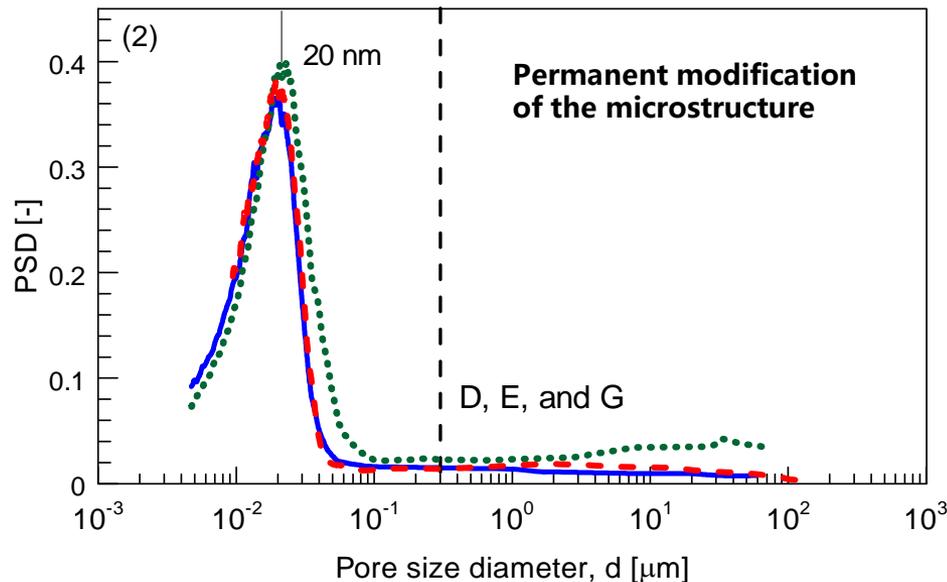
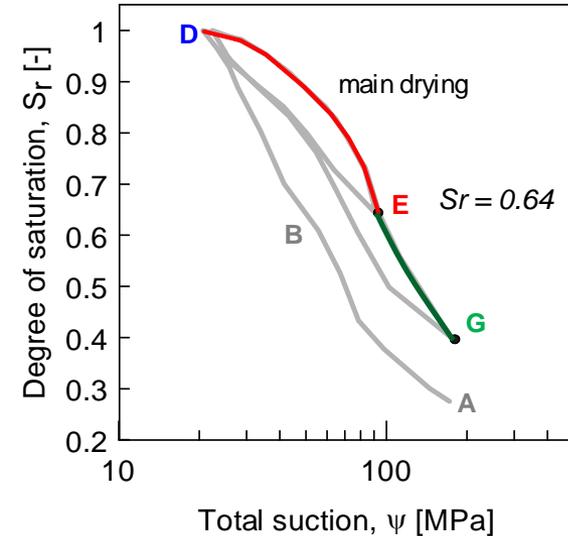
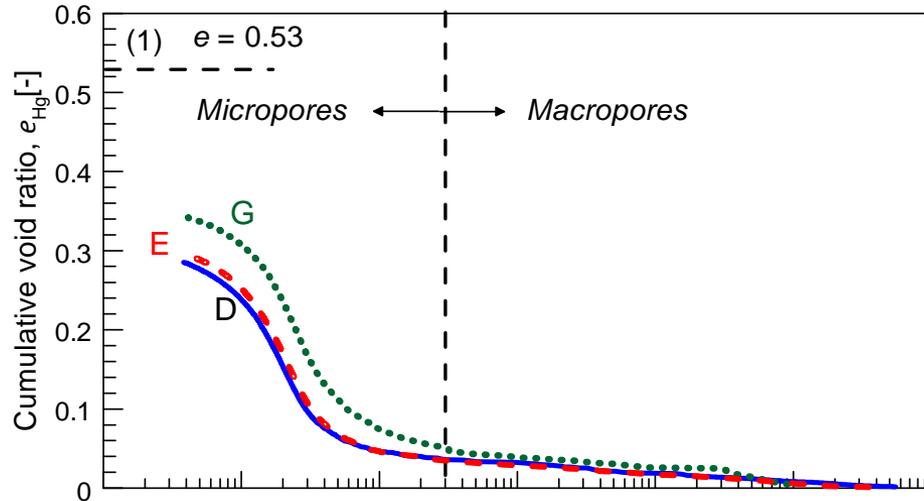
MIP analysis and the influence of wetting/drying on the fabric



- A, as compacted
- - - B, at $S_r = 0.60$
- D, fully saturated

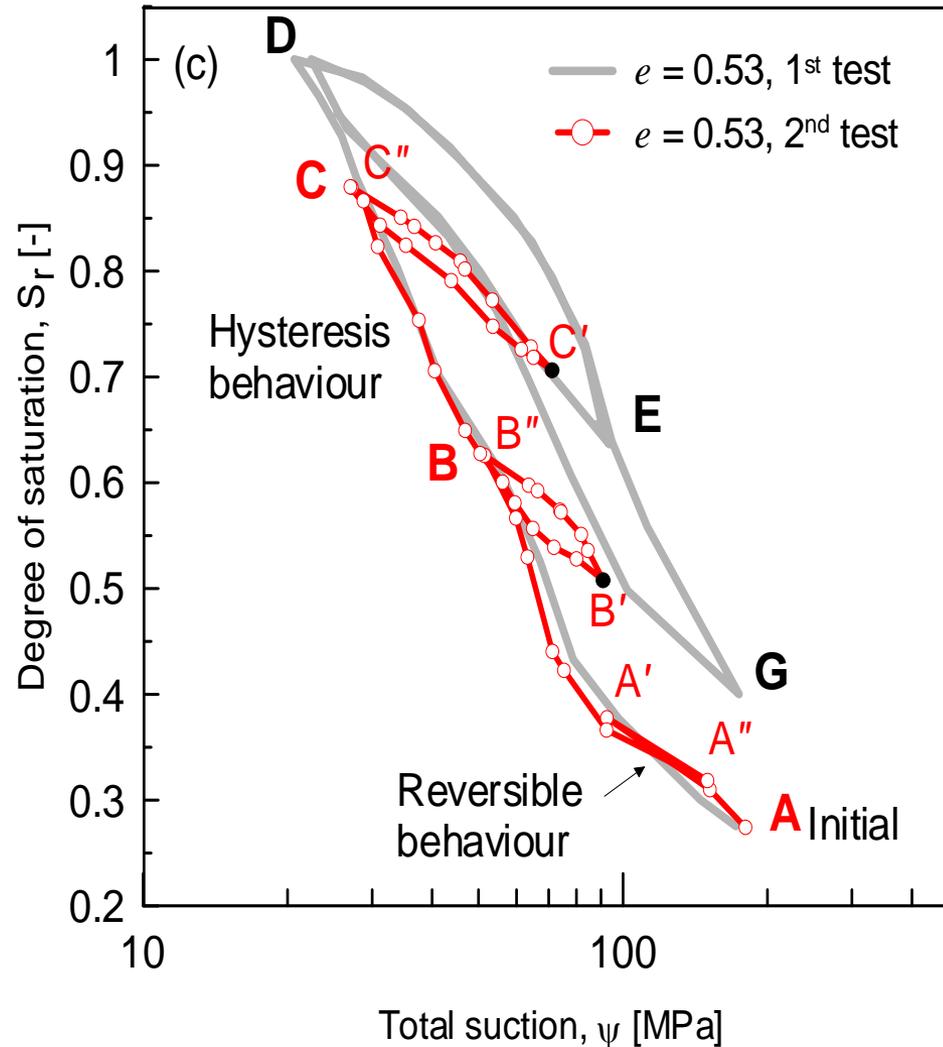
Decomposition of the total
void ratio: $e = e_m + e_M$

MIP analysis and the influence of wetting/drying on the fabric

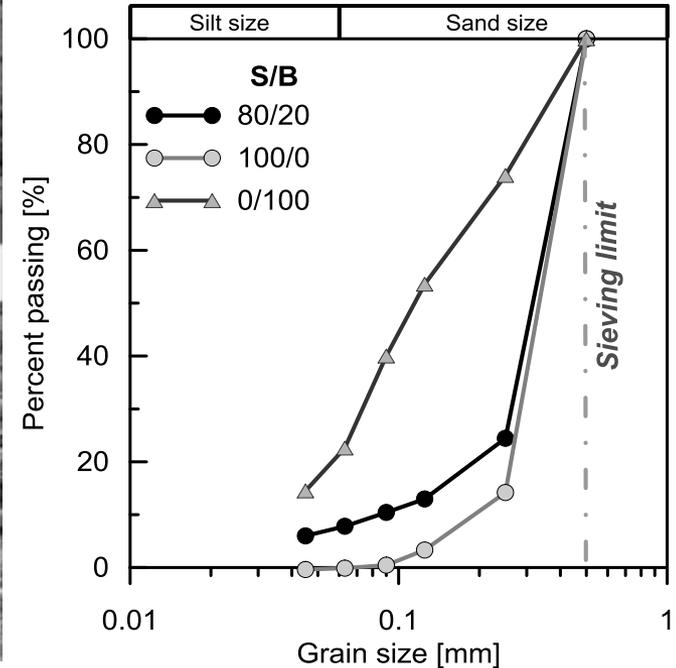
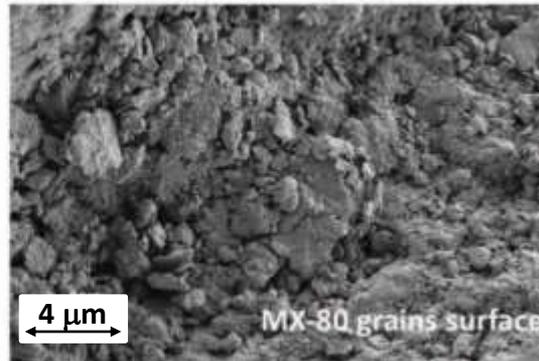
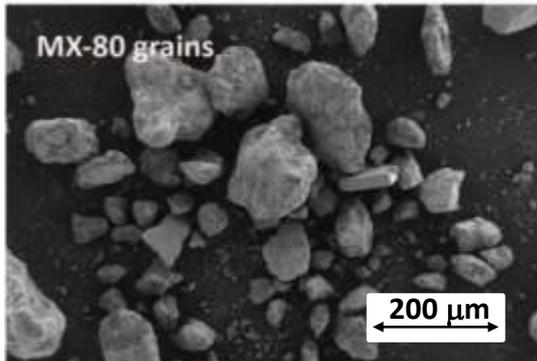
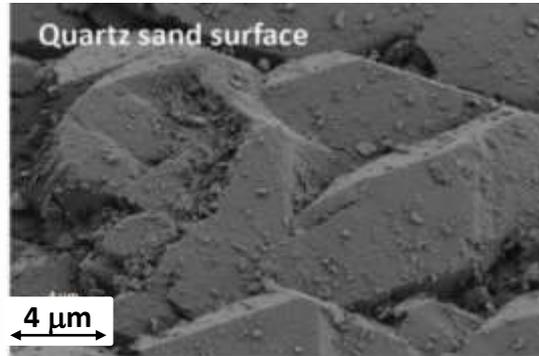
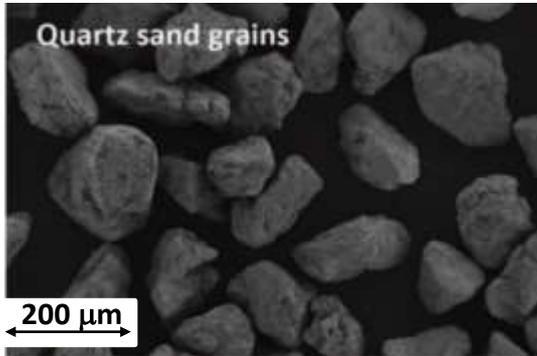


- D, fully saturated
- - - E, at $S_r = 0.64$
- ⋯ G, end of drying

Wetting/drying before the fully saturation of the specimen



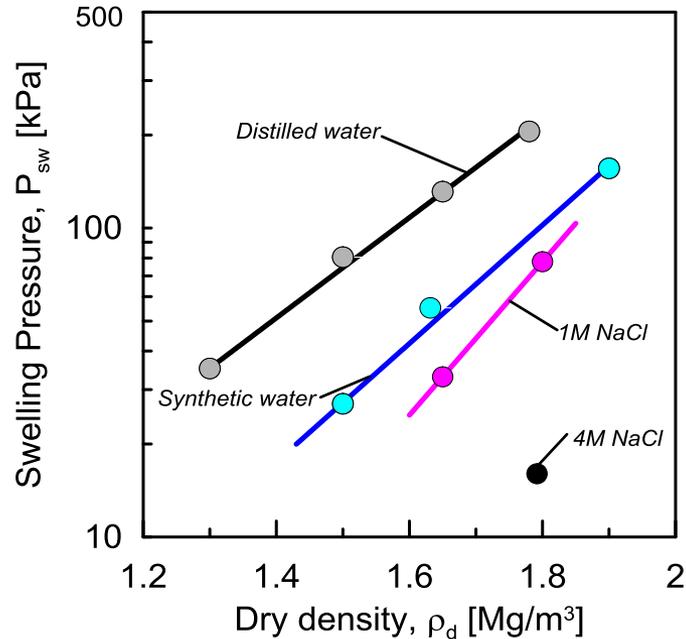
80/20 Sand/Granular Bentonite Mixture:



Properties	Sand	MX-80	80/20 S/B
Particle density, ρ_s [Mg/m ³]	2.65	2.74*	2.67
Liquid limit,	-	420*	81‡
Plastic limit,	-	65*	23.5‡
Smectite content	-	85%†	17%
Specific surface area, S [m ² /g]	0.003	523†	-

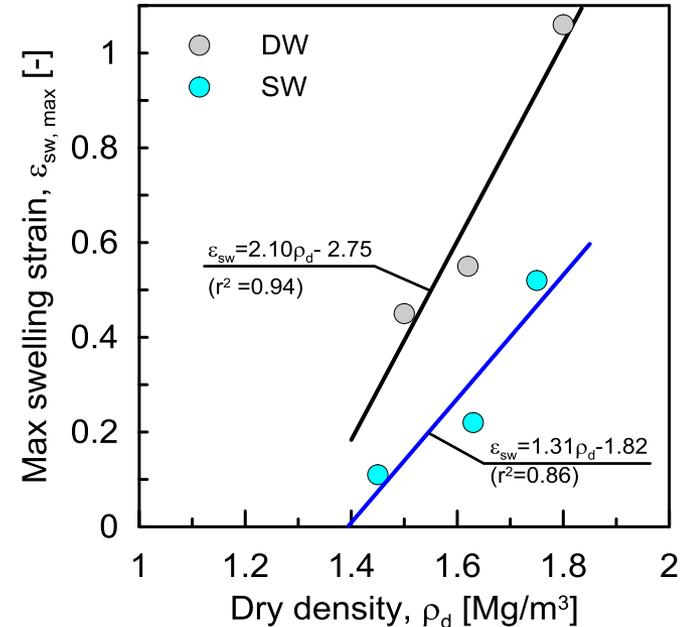
Manca, Ferrari and Laloui (2016)

Constrained swelling test



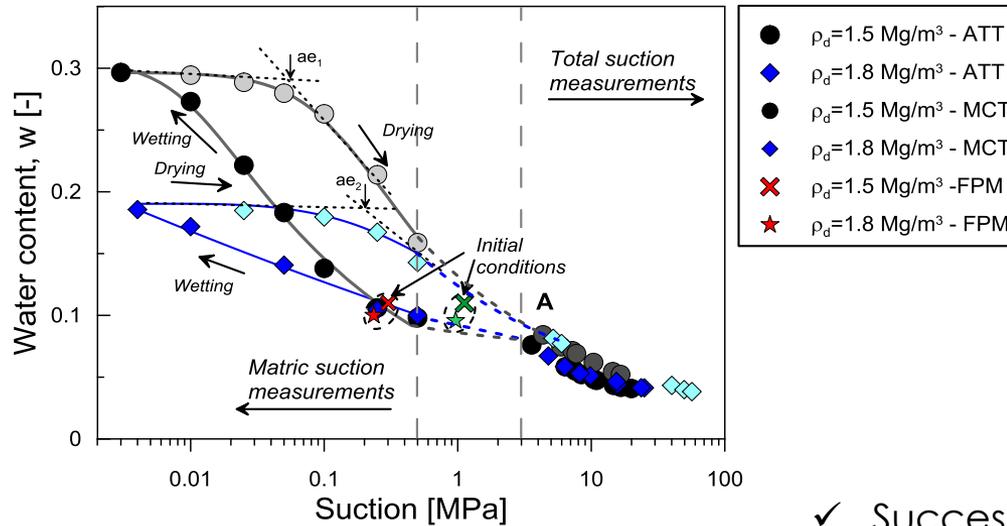
- ✓ Exponential increment of P_{sw}
- ✓ P_{sw} reduction in the range of 67% - 45% for the dry density in the range of 1.3 - 1.9 g/cm³ when the mixture is in contact with SW
- ✓ P_{sw} reduction in the range of 75% - 65% for the dry density in the range of 1.5 - 1.8 g/cm³ when the mixture is in contact with sodium chloride 1M

Free swelling test

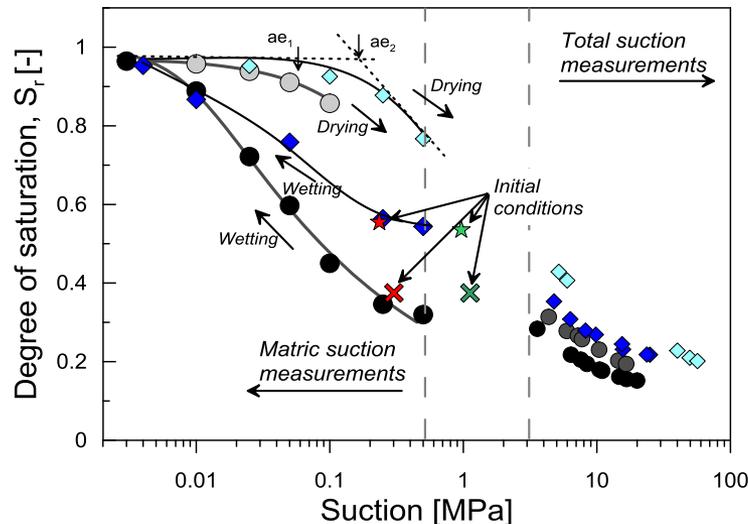


- ✓ Linear increment of the swelling deformation with dry density for both type of waters
- ✓ ϵ_{sw} reduction in the range of 80% - 40% for the dry density in the range of 1.3 - 1.9 g/cm³ when the mixture is in contact with synthetic water

Water retention capacity with distilled water: two dry densities



- ✓ Successful combination of three experimental techniques
- ✓ Slight influence of the compaction density on the initial suction (as-compacted state)
- ✓ Two distinct regions of retention: Adsorption and capillary
- ✓ High density dependence on the low suction zone



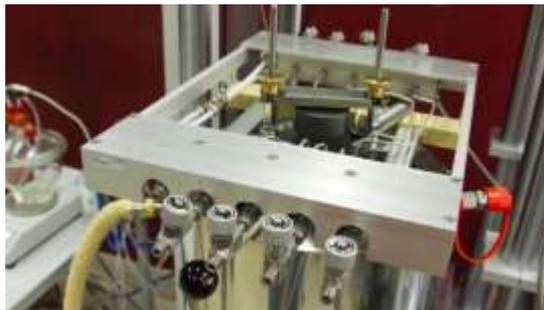
Applications and features



Inner cell system for specimen volume change assessment

At each base :

- Air flushing
- Water flushing
- Pore air pressure control
- Pore **water pressure** control
- **water volume** change measurement



Double PV controller for

- **outer cell** pressure control
- **Inner cell** pressure control
- inner cell **volume change measurement**

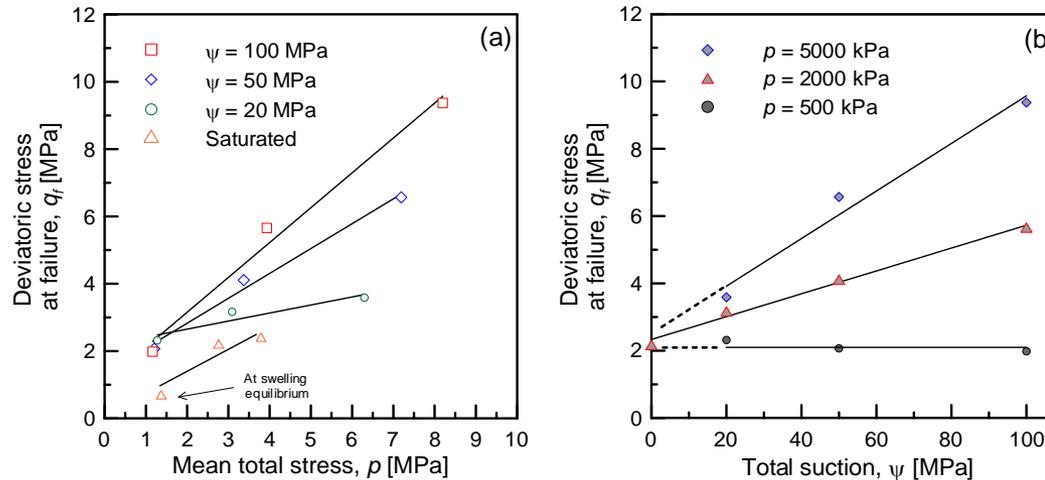
2 PV controllers for the independent control of the pwp at the two bases



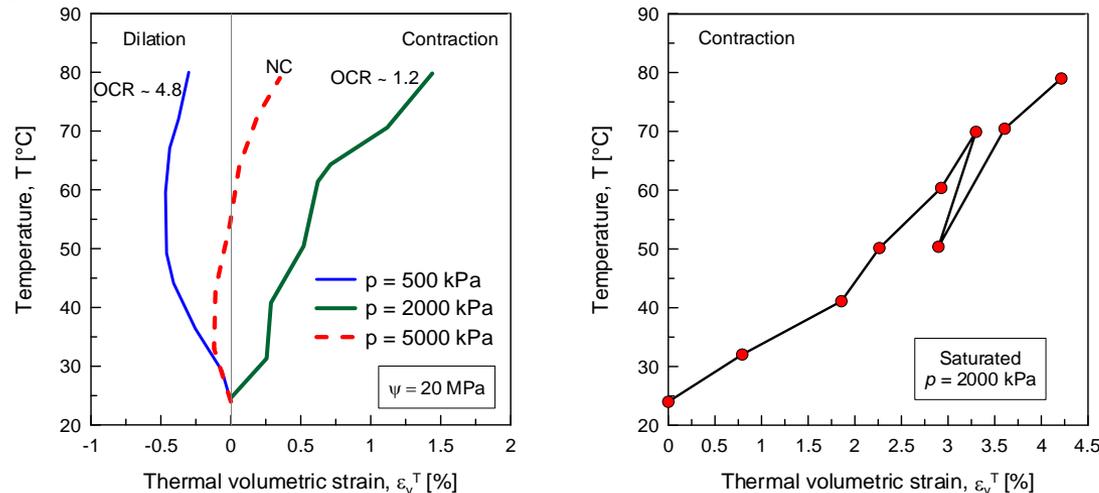
- ✓ Temperature control (4 – 150°C)
- ✓ Maximum confining pressure up to 30 MPa
- ✓ Maximum axial force up to 450 kN (corresponding to 230 MPa axial stress on sample 100x50 mm)
- ✓ Integrated system for matric and total suction control (0 – 1.5 MPa, 4 – 400 MPa)
- ✓ Independent volume/pressure controllers for top and bottom of the sample (permeability measurement)
- ✓ Swelling pressure measurement in constant volume condition
- ✓ Possibility of installation of several local LVDTs inside the cell

Deviatoric response for saturated and unsaturated conditions

Seiphoori (2014)



Influence of temperature on volumetric behaviour of unsaturated and saturated material



† Unsaturated condition after isotropic mechanical compaction

† Saturated condition after isotropic mechanical consolidation

- LMS-EPFL performed detailed characterization studies on different bentonite-based materials (MX-80 Granular Bentonite, MX-80/Sand mixtures, Shot-clay)
- The experimental work focused a wide range of tests including microstructure analysis, water retention response and coupled Thermo-Hydro-Mechanical aspects.
- Some interesting outcomes:
 - ✓ Microstructural observations at different points along the water retention domain provide insights on the behaviour of active clays. Significant change in water retention behaviour of compacted bentonite after first saturation due to the pore structure evolution
 - ✓ The swelling properties of sand-bentonite mixture can be defined from bentonite properties and bentonite fraction.

- A. Seiphoori, A. Ferrari and L. Laloui. *Water retention behaviour and microstructural evolution of MX-80 granular bentonite during wetting and drying cycles*, in *Geotechnique*, vol. 64(9), p. 721-734, 2014.
- L.M. Keller, A. Seiphoori, P. Gasser, F. Lucas, L. Holzer and A. Ferrari. *The pore structure of compacted and partly saturated MX-80 bentonite at different dry densities*, in *Clays and Clay Minerals*, vol. 62(3), p. 174-178, 2014.
- A. Seiphoori, A. Ferrari, J. Rüedi, and L. Laloui. *Shot-clay MX-80 bentonite: An assessment of the hydro-mechanical behavior*, in *Engineering Geology*, vol. 173, p. 10-18 (2014).
- A. Seiphoori, *Thermo-hydro-mechanical characterisation and modelling of MX-80 granular bentonite*, PhD Thesis, EPFL n° 6159, 2014.
- D. Manca, A. Ferrari and L. Laloui. *Fabric evolution and the related swelling behaviour of a sand/bentonite mixture upon hydro-chemo-mechanical loadings*, in *Geotechnique*, vol. 66, num. 1, p. 41-57, 2016.