



**FEBEX-DP**

Full scale engineered barrier experiment - Damskipp project

FEBEX/FEBEX-DP: 1997 - 2014

FEBEX-DP: 2014 - 2016



**BEACON**  
Bentonite Mechanical Evolution

# **FEBEX AND FEBEX-DP PROJECTS AT THE GRIMSEL TEST SITE: ONSITE BENTONITE ANALYSIS**

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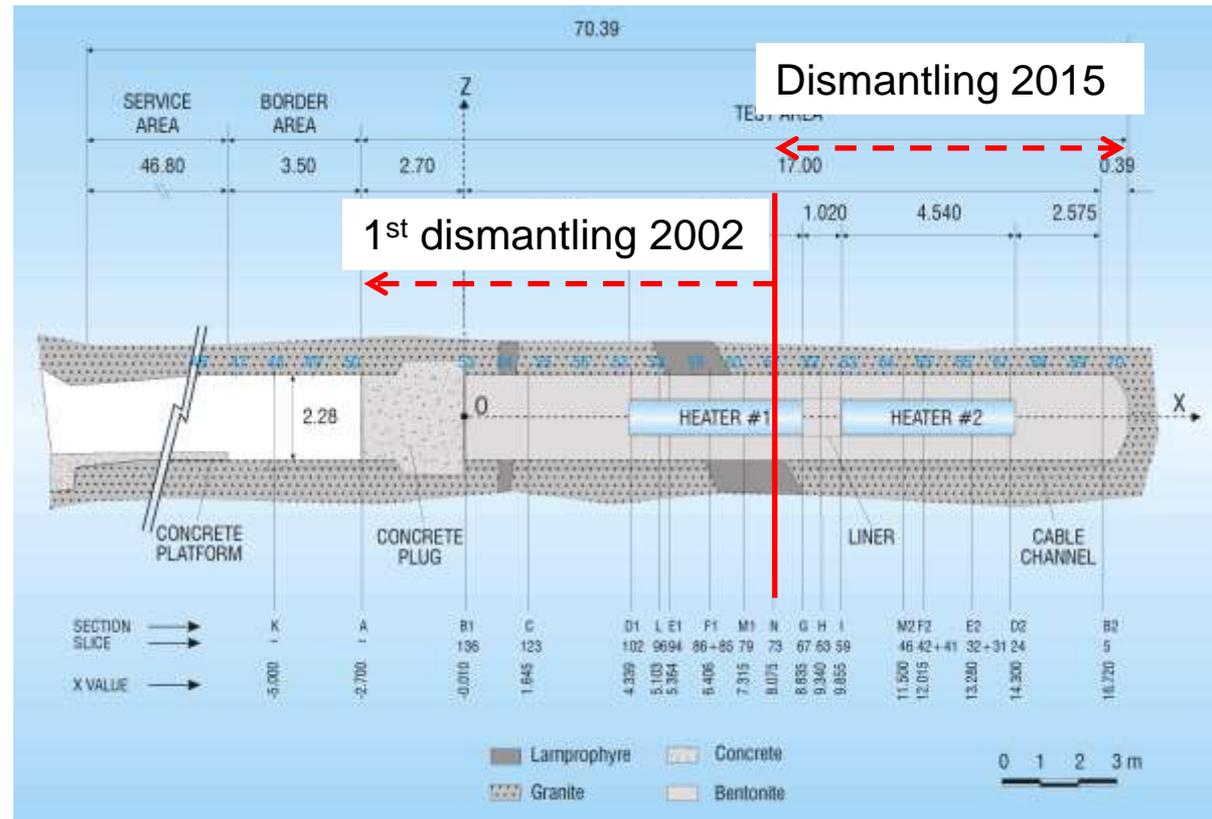


BEACON Workshop “Mechanical properties of bentonite barriers”  
LEI, Kaunas - Lithuania  
June, 19<sup>th</sup> - 20<sup>th</sup> 2017

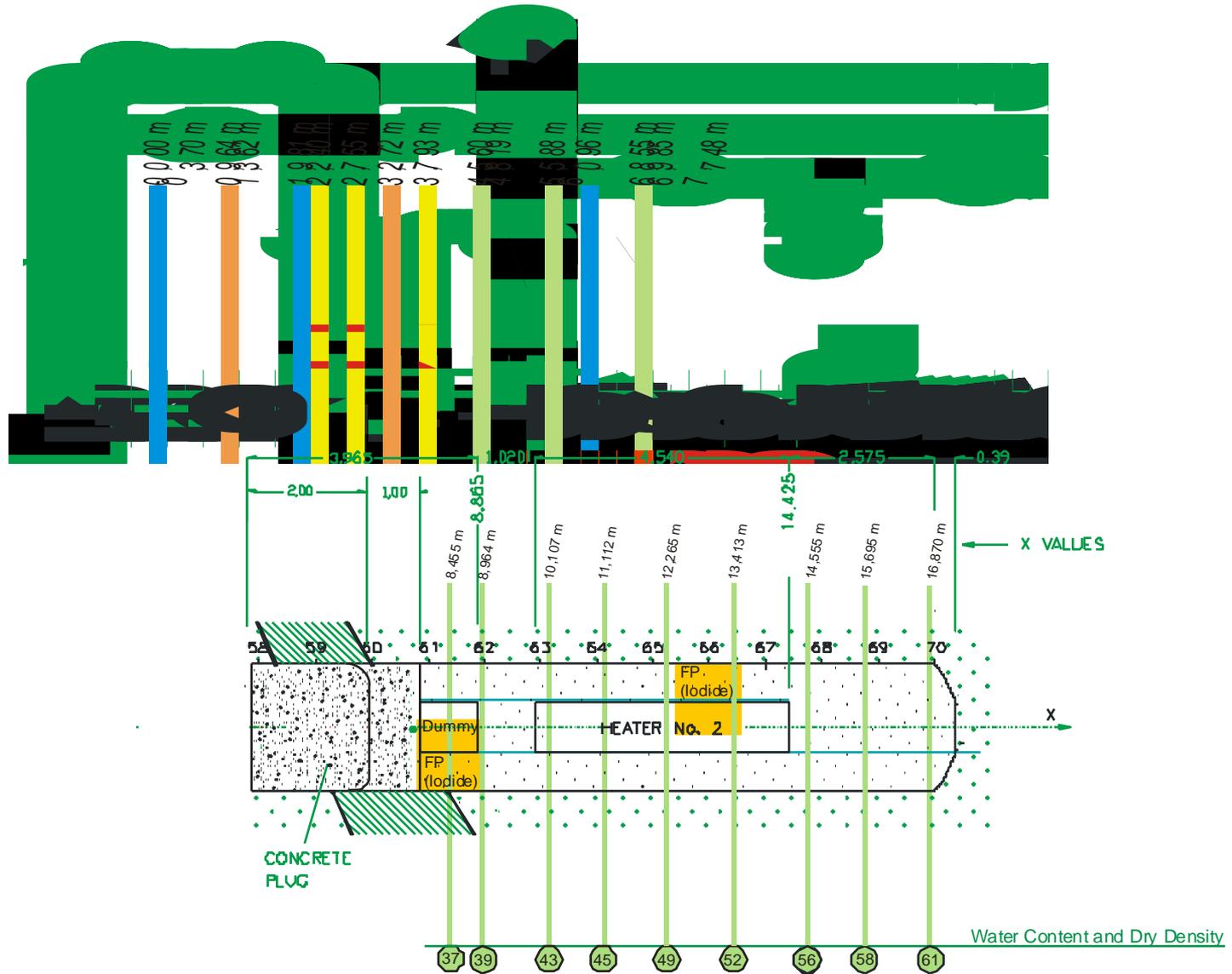
# IN SITU TESTS DISMANTLING DATABASES



- Full-scale in situ test at GTS
- Bentonite blocks barrier, natural hydration, two heaters
- In operation since 1997
- Partial dismantling in 2002
- Final complete dismantling in 2015



# ONSITE DETERMINATION OF WATER CONTENT AND DRY DENSITY

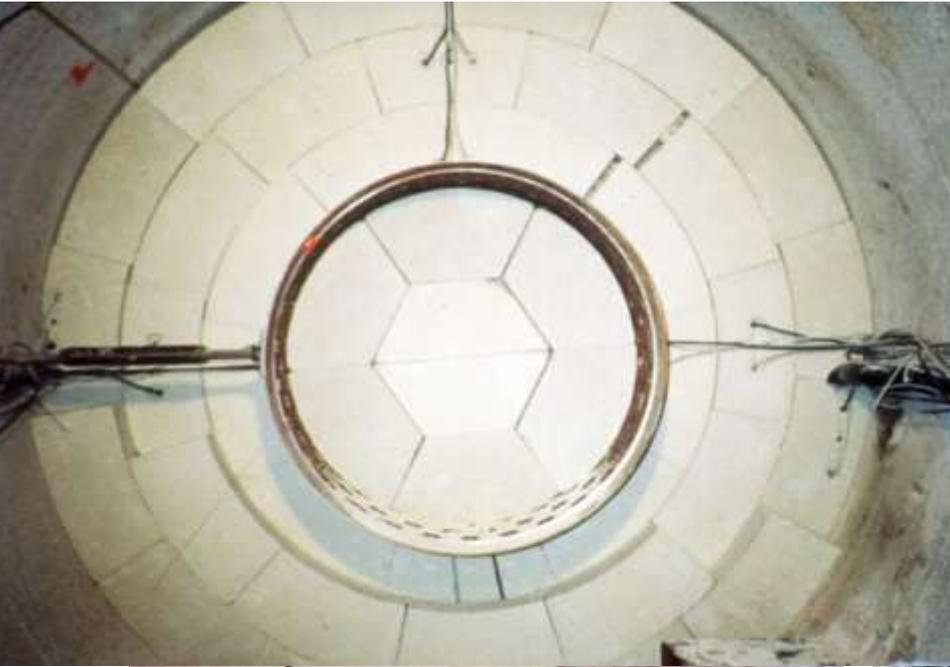


# GAP SEALING



1997

2002

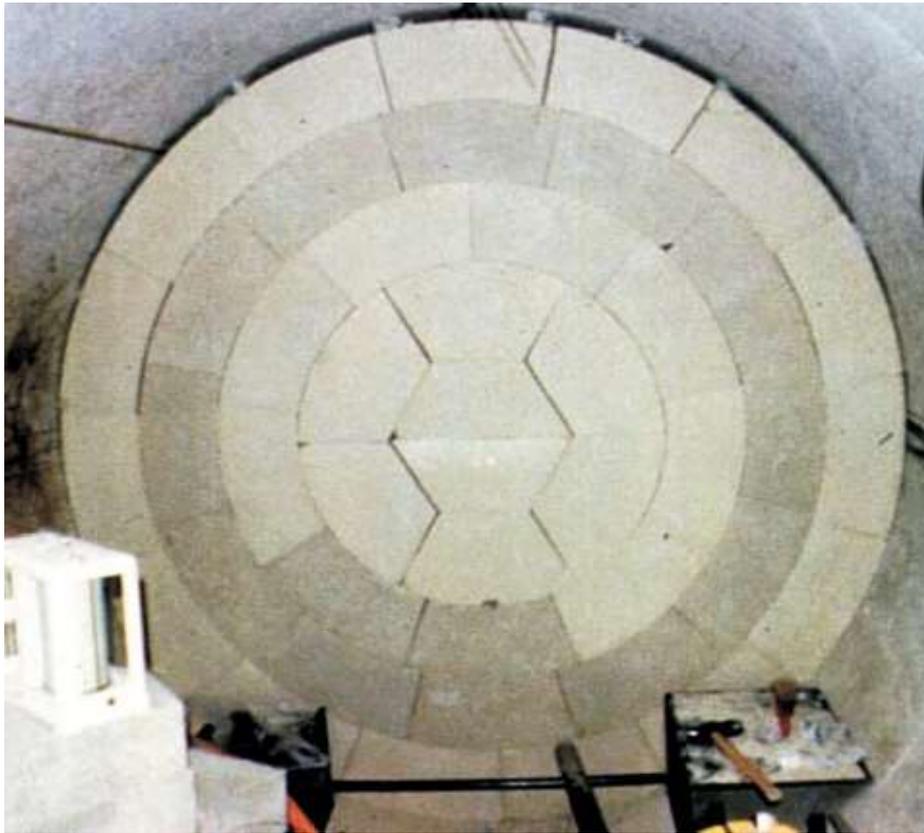


# GAP SEALING



The gaps between blocks had disappeared, as it was already observed in 2002

1997



2015



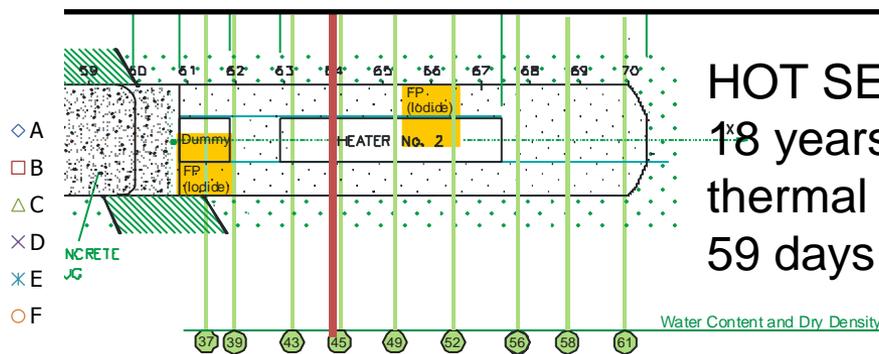
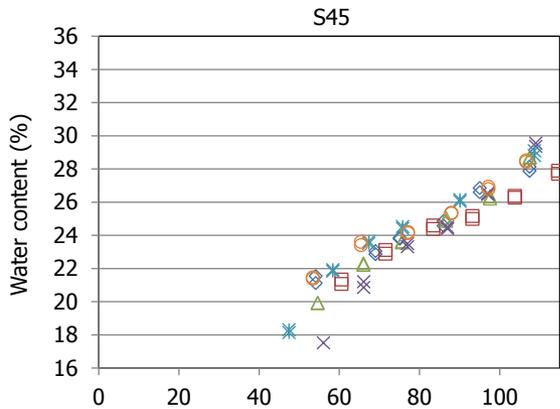
# GAP SEALING



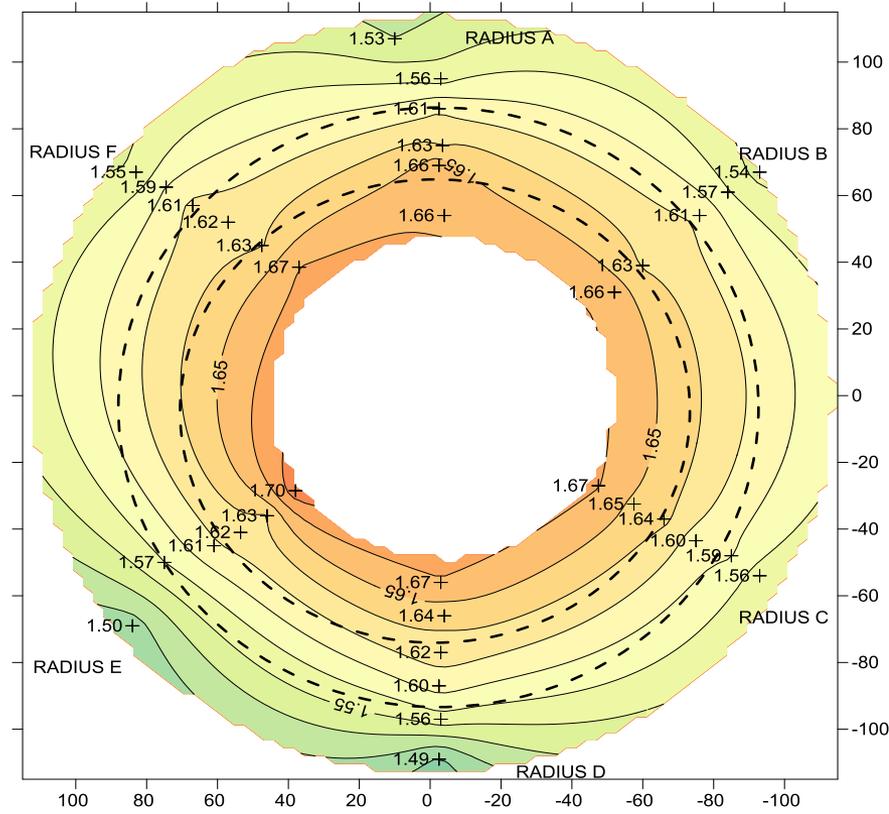
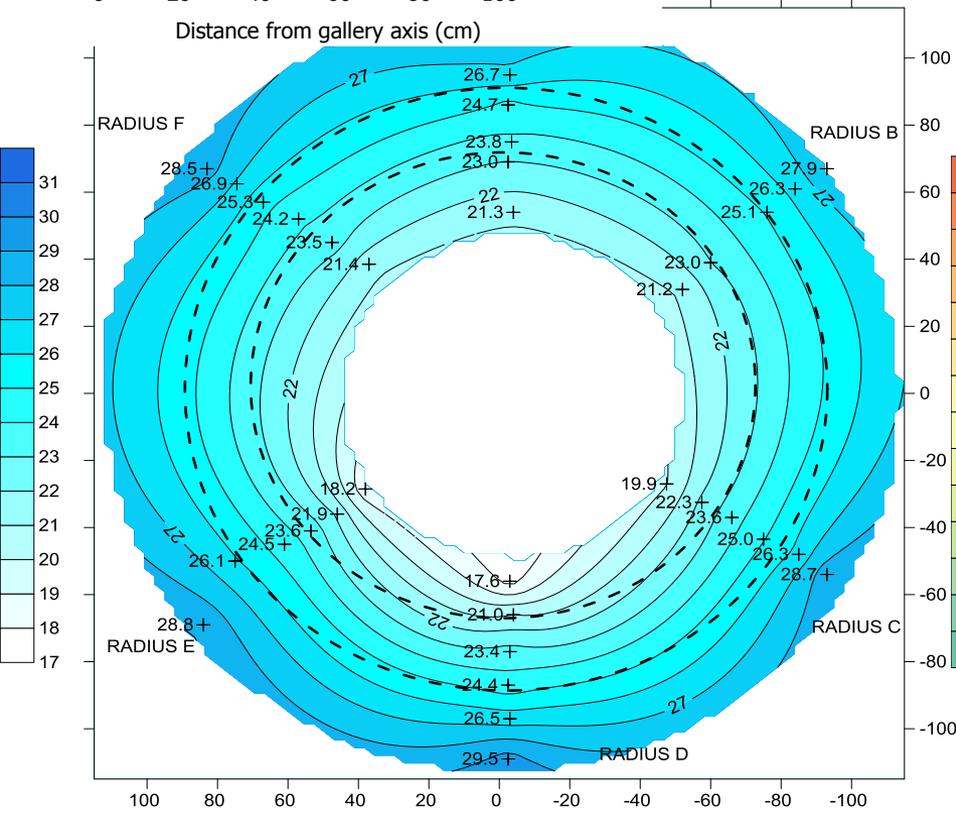
- The gaps between blocks were sealed
- The contact between slices was tight and was not a preferential pathway
- Tight granite/bentonite contact
- This was already observed during first dismantling



# RADIAL PATTERN

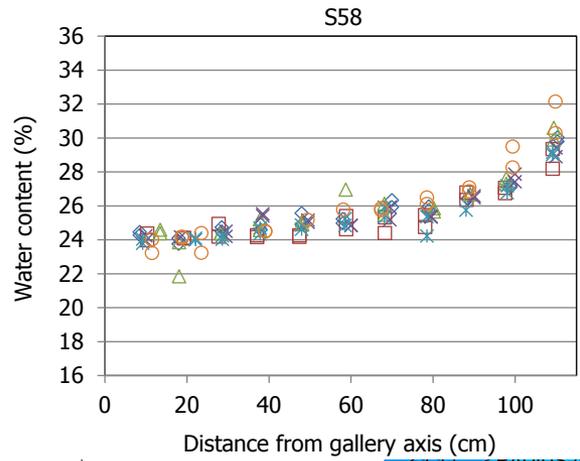


**HOT SECTION (S45)**  
 18 years hydration under  
 thermal gradient (92-35°C)  
 59 days cooling

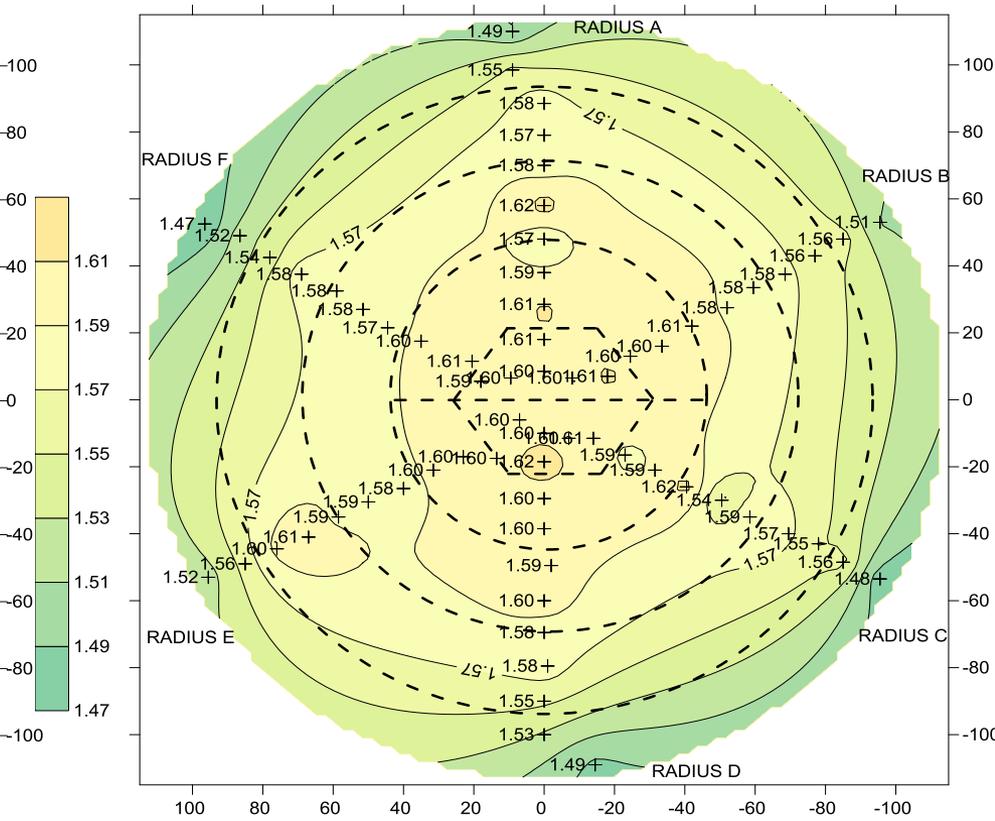
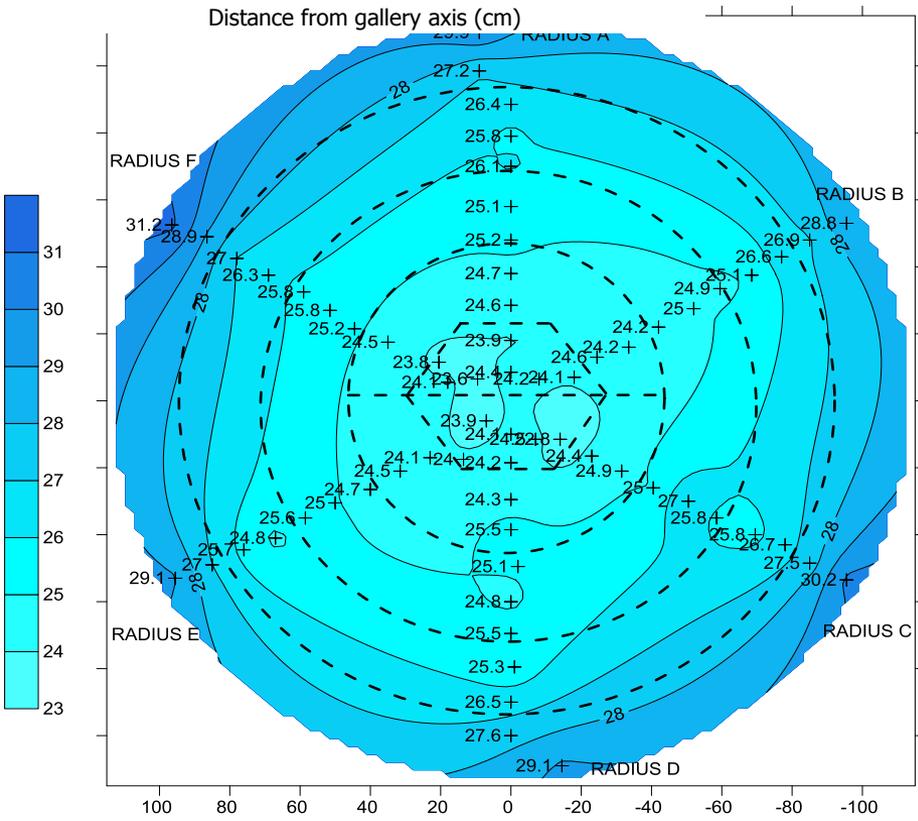




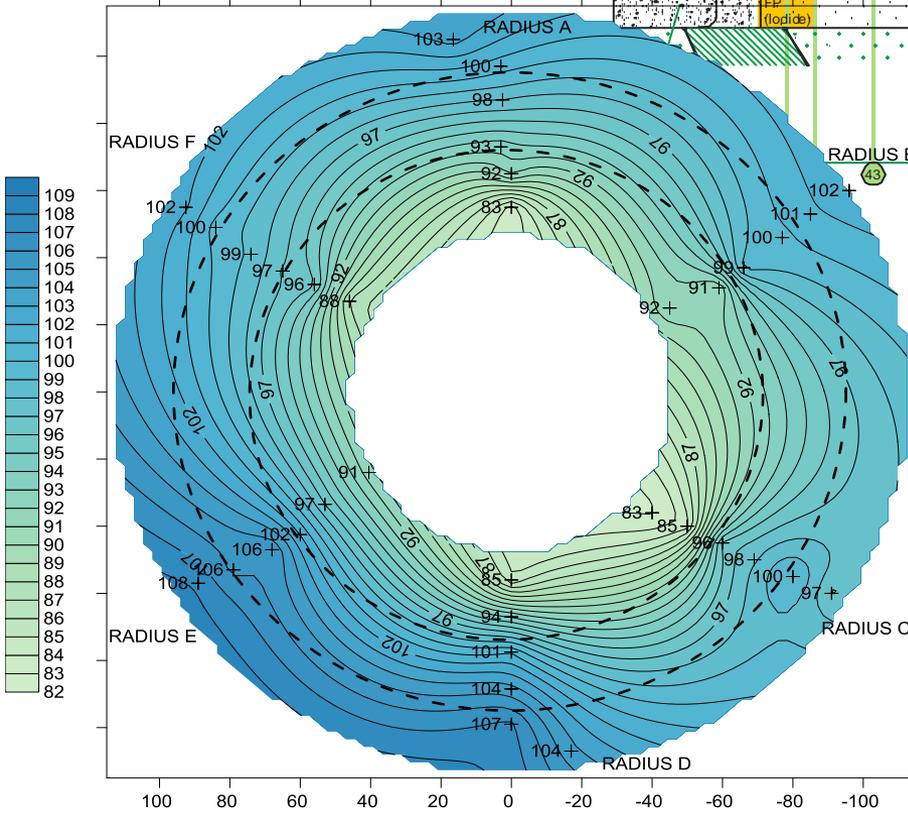
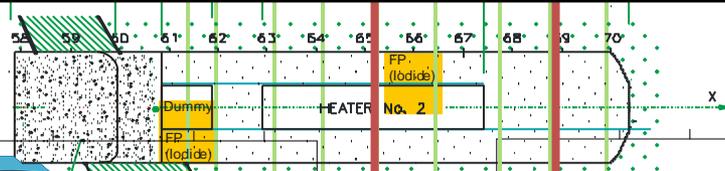
# RADIAL PATTERN



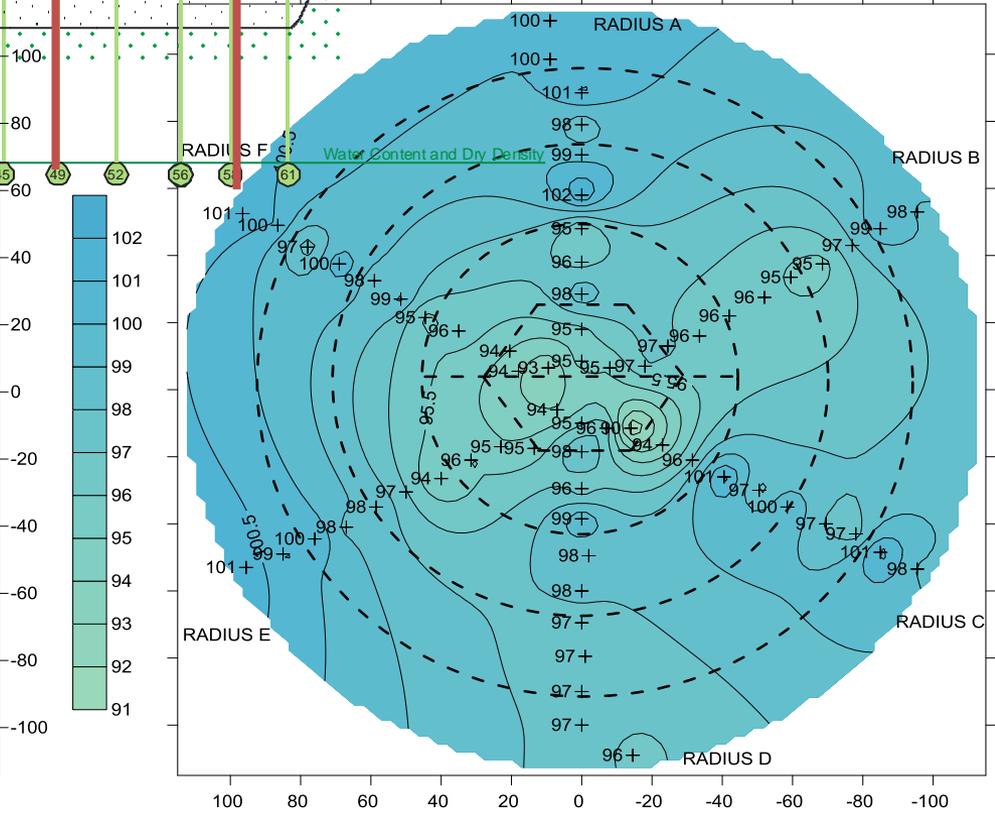
COLD SECTION (S58)  
18 years "warm"  
hydration (>23°C)



# DEGREE OF SATURATION



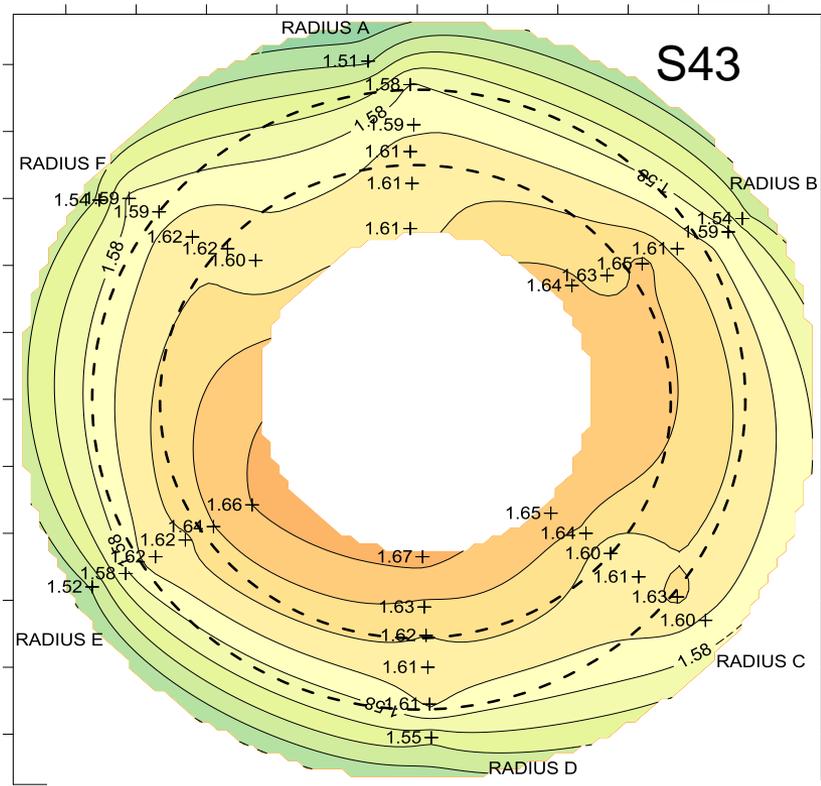
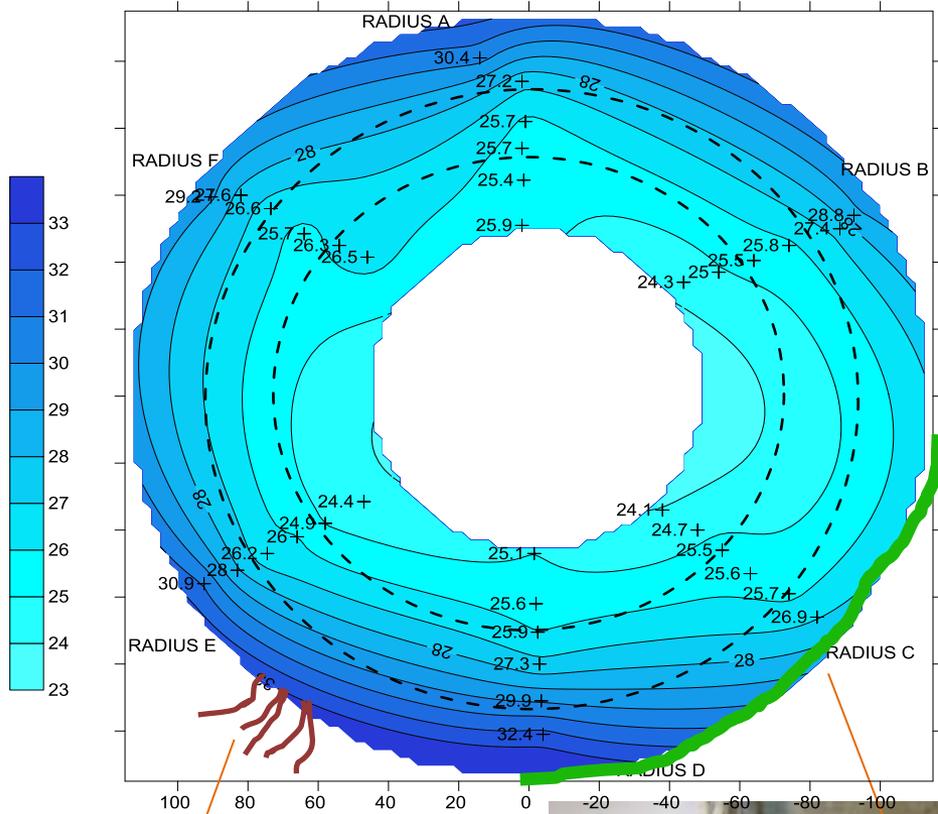
**HOT SECTION (S49)**



**COLD SECTION (S58)**

- Following radial pattern around the heater (always >80%)
- Homogeneous and about 100% in cold sections
- >100% in many samples

# AXIAL SYMMETRY



Filled fractures in granite

Plastic sheet left behind at the bottom left quarter

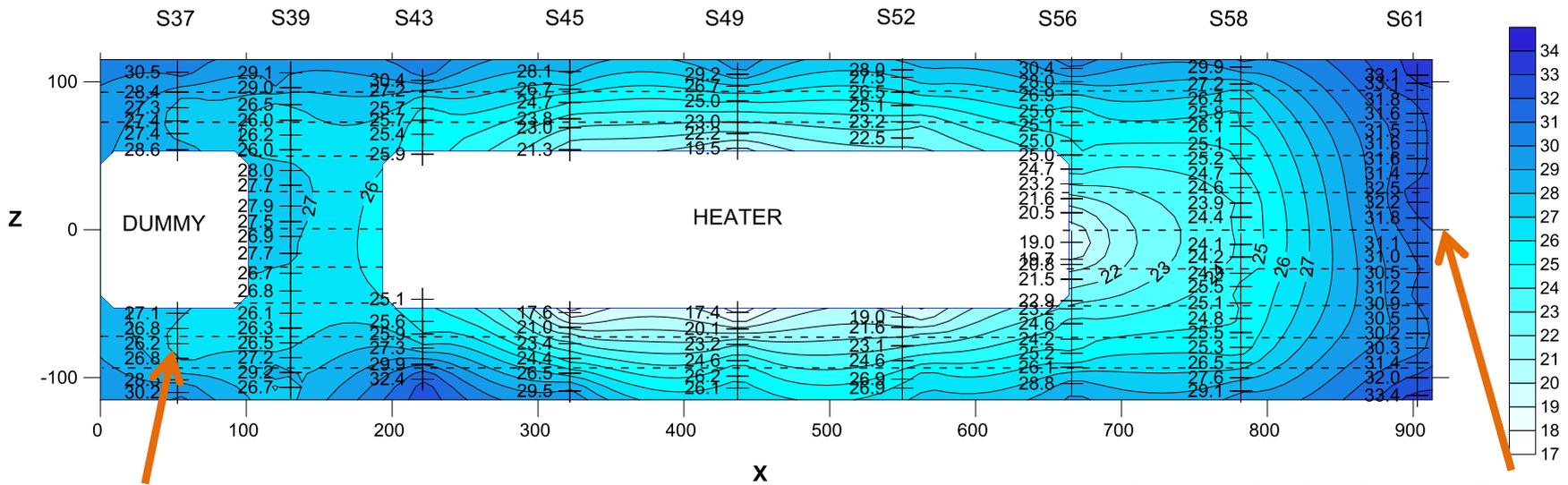


Lower density in upper part: bentonite intrusion through liner holes



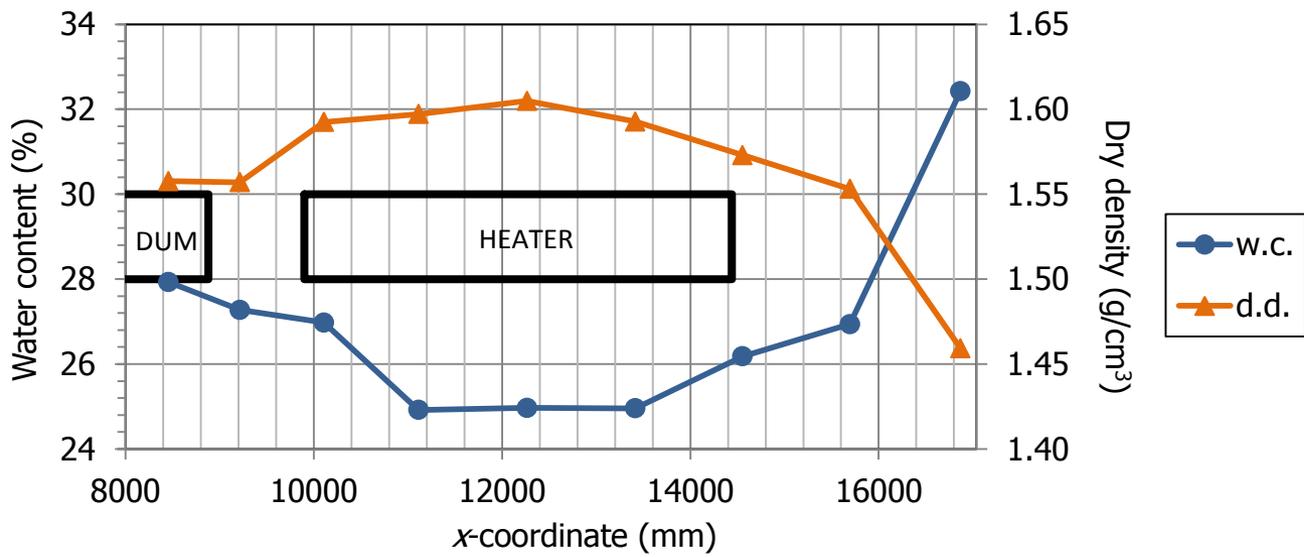


# LONGITUDINAL DISTRIBUTION: WATER CONTENT

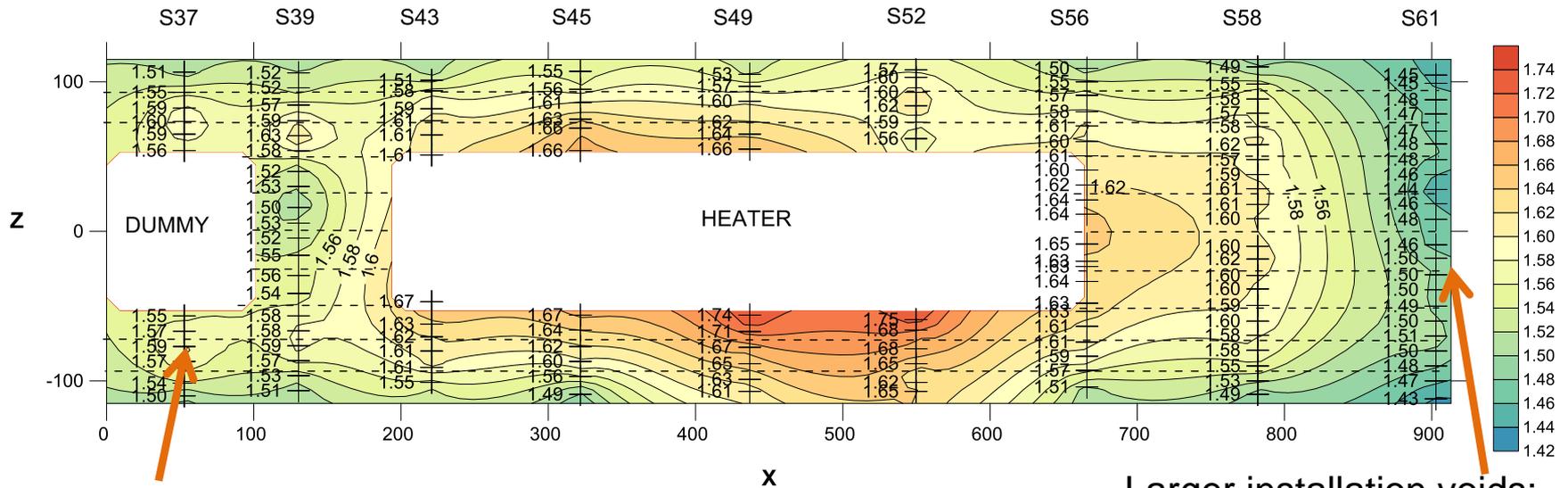


Subjected to thermal gradient for 5 years  
Water from concrete?

Larger hydration surface

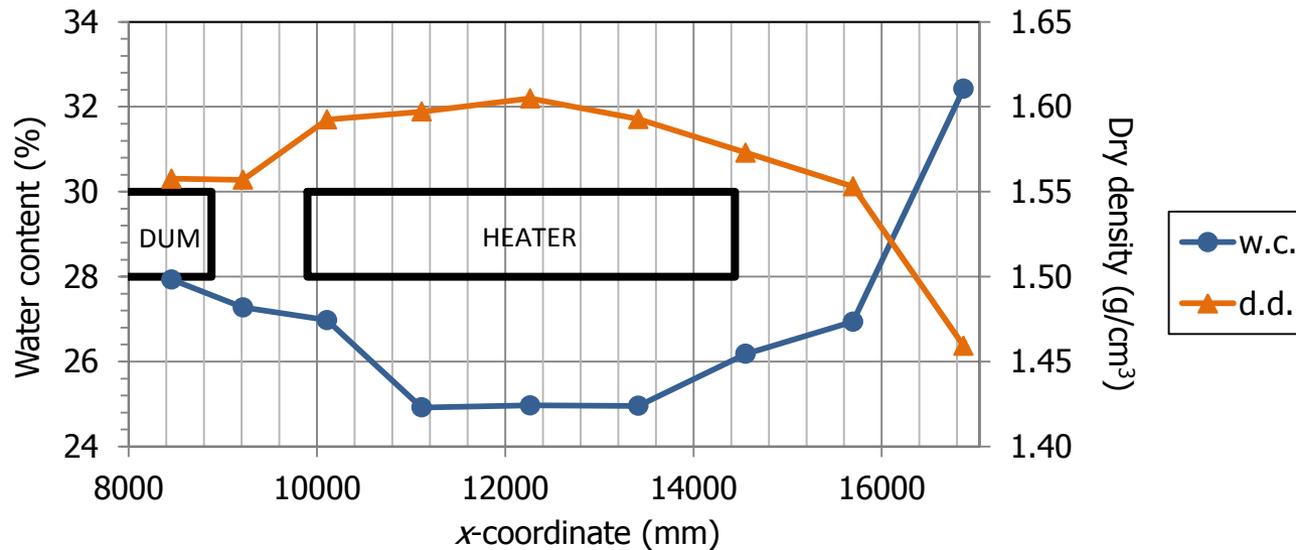


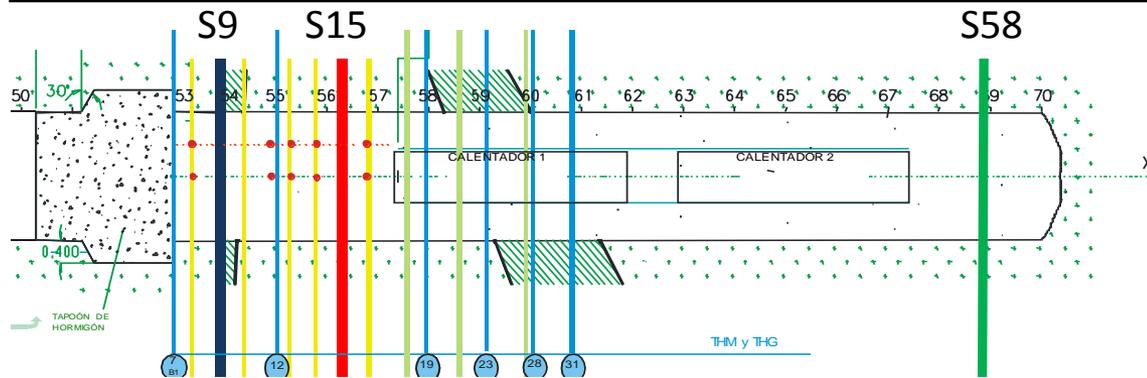
# LONGITUDINAL DISTRIBUTION: DRY DENSITY



Subjected to thermal gradient for 5 years

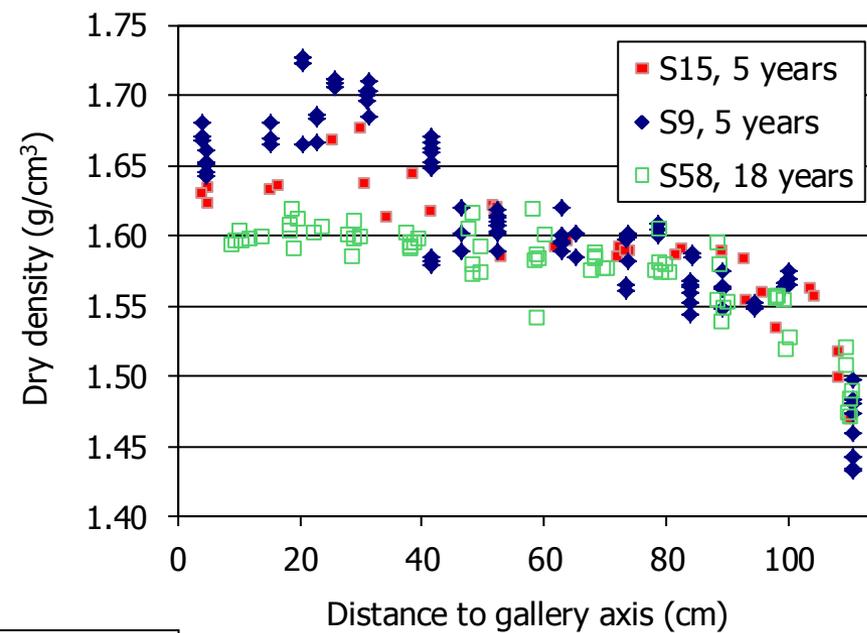
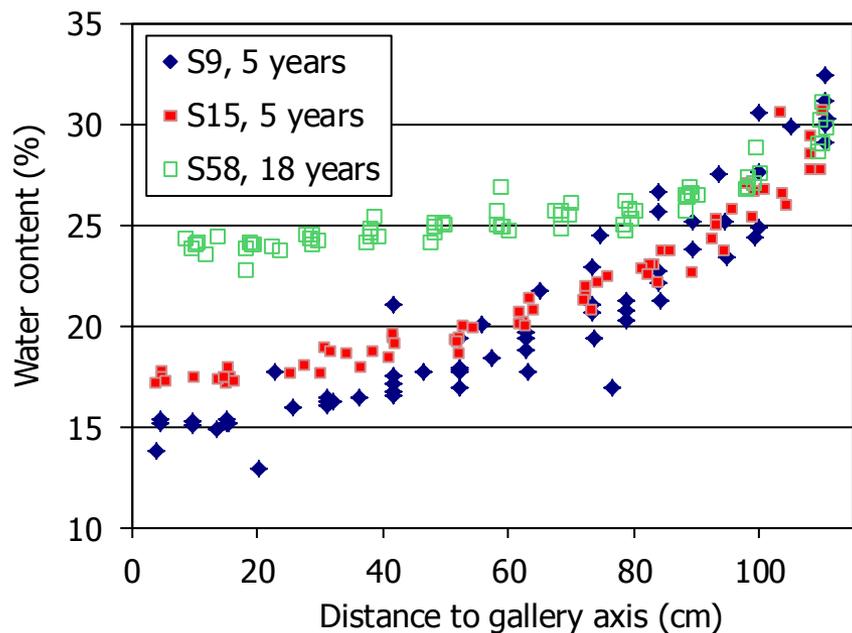
Larger installation voids:  
37% vs. 6%





COLD SECTIONS

COLD SECTIONS



$w$ , %

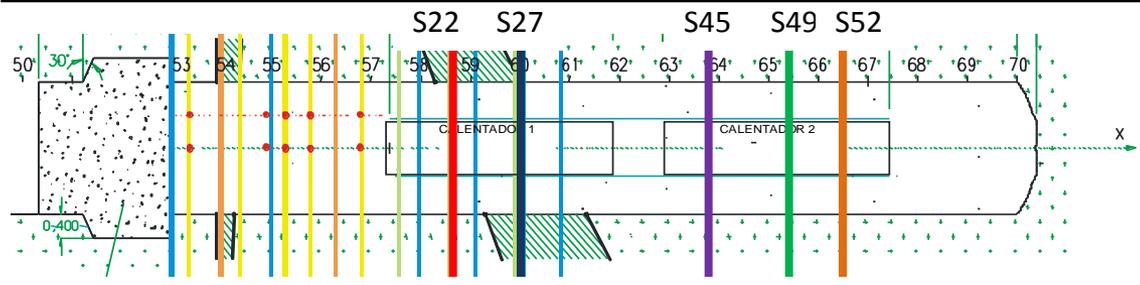
S9: 22.9%  
S15: 22.8%  
S58: 27.1%

$S_r$ , %

S9: 85%  
S15: 86%  
S58: 98%

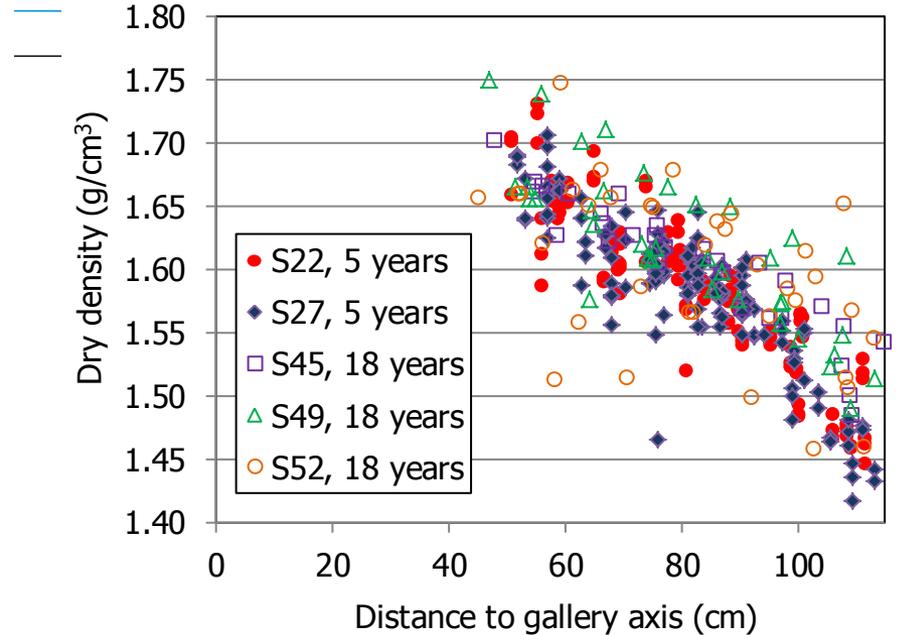
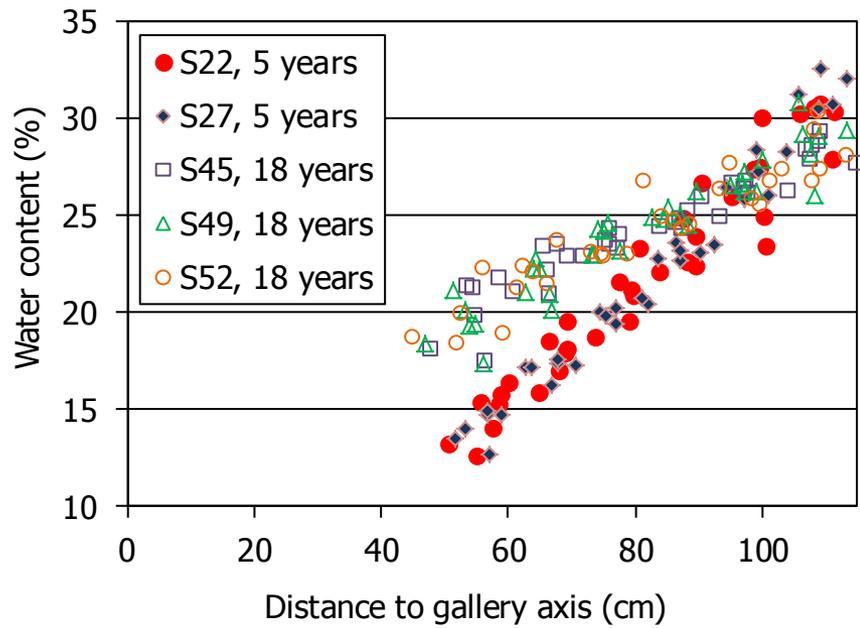
$\rho_d$ , g/cm<sup>3</sup>

S9: 1.58 g/cm<sup>3</sup>  
S15: 1.58 g/cm<sup>3</sup>  
S58: 1.55 g/cm<sup>3</sup>



HOT SECTIONS

HOT SECTIONS



$w, \%$	
S22: 22.6%	S45: 25.7%
S27: 22.6%	S49: 25.9%
	S52: 25.6%

$S_r, \%$	
S22: 85%	S45: 98%
S27: 84%	S49: 99%
	S52: 98%

$\rho_d, \text{g/cm}^3$	
S22: 1.57 g/cm <sup>3</sup>	S45: 1.59 g/cm <sup>3</sup>
S27: 1.56 g/cm <sup>3</sup>	S49: 1.59 g/cm <sup>3</sup>
	S52: 1.59 g/cm <sup>3</sup>

## SUMMARY OF OBSERVATIONS

- ✓ Sealing capacity develops quickly **if water availability is enough**
- ✓ The thermal gradient delays homogenisation, because it **hinders(?)** saturation
- ✓ The dry density changes take place not only radially but also **longitudinally** along the barrier (effect of the back of the gallery)
- ✓ The state in the external part of the barrier barely changed with respect to the first dismantling: **irreversibility** of initial deformation
- ✓ Low density favours homogenisation (**initial strains** are not too large)
- ✓ Homogeneous water content is not imperative for homogeneous  $S_r$ :  
implications on dry density homogenization

# CHANGES DURING DISMANTLING



The state of the barrier just described does not exactly represent the state during operation:

- when the sections were dismantled they had been cooling for periods of time between 24 and 98 days: water redistribution in the internal part of the barrier around the heater → the gradients were steeper
- dry density decreased because of sampling and trimming (sample preparation). The effect is more significant the higher the water content → the overall dry density was higher during operation
- expansion of the front of the barrier after plug demolition → the dry density and degree of saturation of the front sections was higher during operation

## UNCERTAINTIES AND FUTURE WORK

- ✓ Role of thermal gradient on homogenisation
- ✓ Scale effect: homogenisation under thermal gradient was observed in small cells. Is the geometry (radial vs. axial) also a discriminating factor?
- ✓ Changes in water content and density in the barrier condition the THM properties of bentonite (thermal conductivity, permeability, swelling capacity, water retention capacity)
- ✓ Data base generated in FEBEX and FEBEX-DP very valuable for modellers
- ✓ Detailed study of gas and water permeability in FEBEX-DP samples
- ✓ Detailed study of microstructure (MIP and XRD) in FEBEX-DP samples



**FEBEX-DP**

Full scale engineered barrier experiment - Dismantling project  
FEBEX-FEBEXa - 1997 - 2014  
FEBEX-DP - 2014 - 2016

The FEBEX project was financed by ENRESA and the EC Contracts FI4W-CT95-006 and FIKWCT-2000-00016

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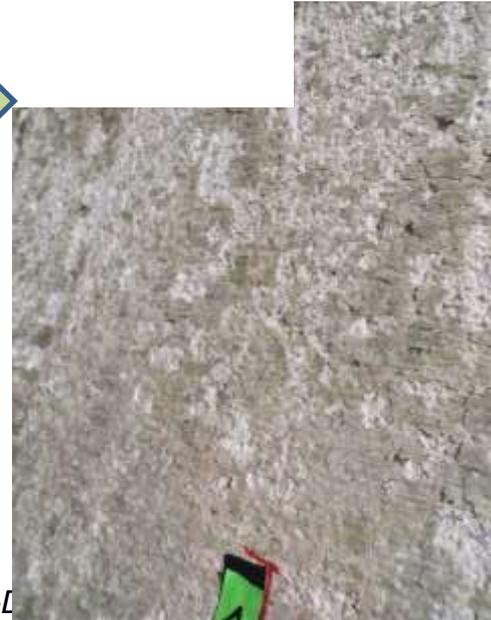
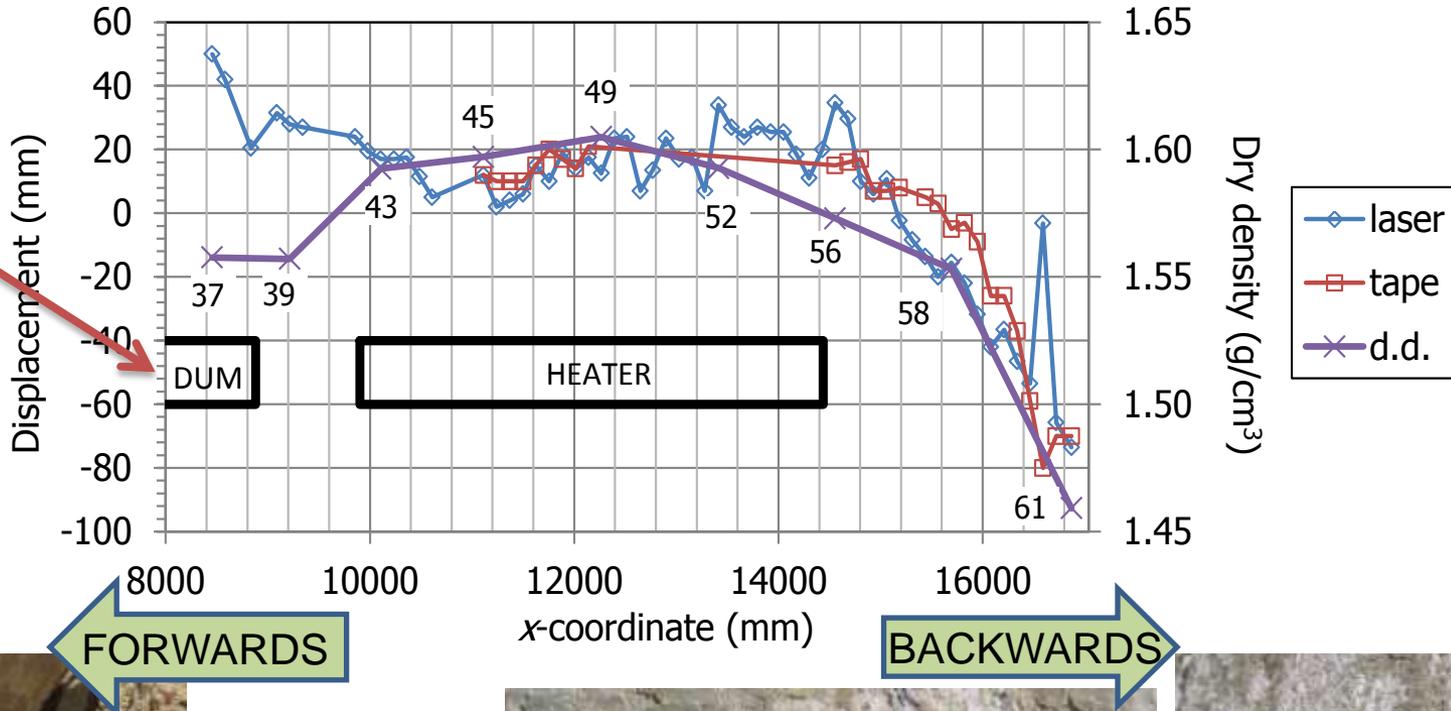
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# LONGITUDINAL DISPLACEMENT



Measurement of the x-coordinate during dismantling: comparison with initial values

Load cell:  
6 MPa



# AVERAGE BARRIER VALUES



$w$ (%)	$\rho_d$ (g/cm <sup>3</sup> )	$S_r$ (%)
25.5	1.59	97

Installation dry density was 1.61 g/cm<sup>3</sup>: this should have not changed during operation (same mass and volume) 

This decrease must be a consequence of sampling (expansion, trimming)

